

NHTSA V2661

Honda Accord LX Broadside Collision With a Narrow Fixed-Object: Foil Test Number 97S003

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FOREWORD

This report documents the test procedures used for and the test results from the first of five broadside crash tests between a 1995 Honda Accord LX four-door sedan and the Federal Outdoor Impact Laboratory (FOIL) 300K instrumented rigid pole. The test was conducted at the Federal Highway Administration (FHWA) FOIL located at the Turner-Fairbank Highway Research Center (TFHRC). The National Highway Traffic Safety Administration (NHTSA) enlisted the FHWA, specifically the FOIL, to aid in the development of laboratory test procedures to be used in an amended version of Federal Motor Vehicle Safety Standard (FMVSS) 201. The amendment would include a 90 degree broadside collision between a passenger vehicle and a narrow fixed object. This new test procedure could be used in the evaluation of dynamic side-impact protection systems (e.g. air bags). One SID/HIII dummy was placed in the driver seat to measure occupant response data. The vehicles were placed on the FOIL's dual rail side-impact system, which was extended to within 0.3 m of the rigid pole to ensure impact location, speed, and SIDH3 stability.

This report (FHWA-RD-98-008) contains test data, photographs taken with high-speed film, and a summary of the test results. The target test speed for this test was 29 km/h.

This report will be of interest to all State departments of transportation; FHWA headquarters; region and division personnel; and highway safety researchers interested in the crashworthiness of roadside safety hardware.



A. George Ostensen, Director
Office of Safety and Traffic
Operations Research and Development

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Technical Report

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16. Abstract This report contains the test procedures, test setup and test results from the first of five broadside crash tests between a 1995 Honda Accord LX four-door sedan and the Federal Outdoor Impact Laboratory (FOIL) 300K instrumented rigid pole. The test was conducted at the Federal Highway Administration (FHWA) FOIL located at the Turner-Fairbank Highway Research Center (TFHRC) in McLean, Virginia. The National Highway Traffic Safety Administration (NHTSA) enlisted the FHWA to aid in the development of laboratory test procedures to be used in an amended version of Federal Motor Vehicle Safety Standard (FMVSS) 201 (Occupant Protection in Interior Impact). This new test procedure could be used in the evaluation of dynamic side-impact protection systems (e.g. air bags). Steps were taken to ensure accurate, repeatable test procedures so that test facilities abroad would achieve similar results given comparable test conditions. The NHTSA supplied a calibrated SID/HIII dummy. The head injury criteria (HIC) and thoracic trauma index (TTI) values were used to determine the severity of the test and as a comparison between subsequent broadside tests to evaluate the repeatability of the test procedures.			
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SI* (MODERN METRIC) CONVERSION FACTORS

APPROXIMATE CONVERSIONS TO SI UNITS

Symbol	When You Know	Multiply By	To Find	Symbol	When You Know	Multiply By	To Find	Symbol
LENGTH								
in	inches	25.4	millimeters	mm	mm	0.039	inches	in
ft	feet	0.305	meters	m	m	3.28	feet	ft
yd	yards	0.914	meters	m	m	1.09	yards	yd
mi	miles	1.61	kilometers	km	km	0.621	miles	mi
AREA								
in ²	square inches	645.2	square millimeters	mm ²	square millimeters	0.0016	square inches	in ²
ft ²	square feet	0.093	square meters	m ²	square meters	10.764	square feet	ft ²
yd ²	square yards	0.836	square meters	m ²	square meters	1.195	square yards	yd ²
ac	acres	0.405	hectares	ha	hectares	2.47	acres	ac
mi ²	square miles	2.59	square kilometers	km ²	square kilometers	0.386	square miles	mi ²
VOLUME								
fl oz	fluid ounces	29.57	milliliters	mL	milliliters	0.034	fluid ounces	fl oz
gal	gallons	3.785	liters	L	liters	0.264	gallons	gal
ft ³	cubic feet	0.028	cubic meters	m ³	cubic meters	35.71	cubic feet	ft ³
yd ³	cubic yards	0.765	cubic meters	m ³	cubic meters	1.307	cubic yards	yd ³
NOTE: Volumes greater than 1000 l shall be shown in m³.								
MASS								
oz	ounces	28.35	grams	g	grams	0.035	ounces	oz
lb	pounds	0.454	kilograms	kg	kg	2.202	pounds	lb
T	short tons (2000 lb)	0.907	megagrams (or "metric ton")	Mg (or "t")	Mg (or "t")	1.103	short tons (2000 lb)	T
TEMPERATURE (exact)								
°F	Fahrenheit temperature	5(F-32)/9 or (F-32)/1.8	Celcius temperature	°C	Celcius temperature	1.8C + 32	Fahrenheit temperature	°F
ILLUMINATION								
fc	foot-candles	10.76	lux	lx	lux	0.0929	foot-candles	fc
fl	foot-Lamberts	3.426	candela/m ²	cd/m ²	cd/m ²	0.2919	foot-Lamberts	fl
FORCE and PRESSURE or STRESS								
lbf	poundforce	4.45	newtons	N	newtons	0.225	poundforce	lbf
lb/ft ²	poundforce per square inch	6.89	kilopascals	kPa	kilopascals	0.145	poundforce per square inch	lb/ft ²

* SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380.

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INTRODUCTION

The National Highway Traffic Safety Administration (NHTSA) enlisted the Federal Highway Administration (FHWA), specifically the Federal Outdoor Impact Laboratory (FOIL), to aid in the development of laboratory test procedures to be used in an amended version of Federal Motor Vehicle Safety Standard (FMVSS) 201 (Occupant Protection in Interior Impact).⁽¹⁾ The amendment would include a 90 degree broadside collision between a passenger vehicle and a narrow fixed-object. This new test procedure could be used in the evaluation of dynamic side impact protection systems (e.g. air bags).

Steps were taken to ensure accurate, repeatable test procedures so that test facilities abroad would achieve similar results given comparable test conditions. The series of tests conducted at the FOIL were broadside collisions between 1995 Honda Accord LX four-door sedans and the FOIL's 300K rigid pole. The vehicles were placed on the FOIL's dual rail side-impact system with the vehicle longitudinal centerline perpendicular to the rigid pole centerline. The two rails used for side-impact at the FOIL were extended to approximately 0.3 m from the rigid pole. This provided accuracy of the impact location as well as repeatability of the impact speed. One SID/HIII dummy was placed in the driver seat to measure occupant response data. The SID/HIII is a combination of the current side-impact dummy (SID) used in side-impact testing and the HYBRID III (HIII) dummy used for frontal-impact testing. This report documents procedures followed and test results from one of four crash tests conducted in support of the FMVSS 201 amendment.

SCOPE

This report documents the results from the first of five broadside crash tests between a 1995 Honda Accord LX four-door sedan and the FOIL 300K instrumented rigid pole. The test was conducted at the FHWA's FOIL located at the Turner-Fairbank Highway Research Center (TFHRC) in McLean, Virginia. The FOIL utilizes a drop tower system for propulsion and two steel rails bolted to a concrete runway for vehicle guidance during broadside testing. The rails were extended to within 0.3 m of the rigid pole to ensure impact location, speed, and SID/HIII stability. The concept of the vehicle remaining on the two rails raised some concern. The concern was that the rails would impede the natural collapse or crush of the vehicle and thus interfere with the accuracy of SID/HIII data. However, the intent of these tests was to develop a procedure for head protection system evaluation and it was believed that the event of interest (dummy contact with the pole) would be complete before significant crush of the vehicle. The procedures followed for vehicle preparation, instrumentation, dummy preparation, and dummy seating procedures are outlined in FMVSS 214.⁽²⁾ The NHTSA supplied a calibrated

SID/HIII dummy for the crash test. Head injury criteria (HIC) and thoracic trauma index (TTI) calculations were performed on the data from the SID/HIII's head and thorax accelerometers. The HIC and TTI values were used to determine the severity of the test and to compare subsequent broadside tests to evaluate the repeatability of the test procedures.

TEST MATRIX

One broadside crash test involving a 1995 Honda Accord LX four-door sedan and FOIL's instrumented 300K rigid pole was conducted. The target vehicle test weight was intended to be between the vehicle curb weight (empty, as received from the dealership) and the fully loaded weight (curb weight plus ballast to simulate the vehicle cargo capacity and one SID/HIII). The target test speed for this test was 29 km/h. The rigid pole was installed with its centerline aligned with the center-of-gravity (cg) of the SID/HIII's head. Table 1 outlines the pertinent test parameters of the broadside crash test.

Table 1. Test matrix.	
FOIL number	97S003
Date	May 28, 1997
Vehicle	1995 Honda Accord
Weight (total)	1,470 kg
SID/HIII Modified neck bracket	One positioned in driver seat HYBRID III neck
Fuel tank	91% capacity with stoddard solvent
Crab angle	90°
Speed (nominal)	29 km/h
Impact location	Pole aligned with SID/HIII head
Test article	FOIL 300K instrumented rigid pole

TEST VEHICLE

The test vehicle was a 1995 Honda Accord four-door sedan with front wheel drive, an automatic transmission, and a four cylinder 2.2 L motor. Table 2 describes the vehicle and optional equipment.

Table 2. Vehicle description and statistics.					
Vehicle make			Honda		
Vehicle model			1995 Accord LX		
Vehicle identification number (VIN)			1HGCD5638SA033570		
Engine			2.2 L, 4 cylinder		
Transmission			Automatic		
Drive chain			Front wheel drive		
Wheel base			2,718 mm		
Wheel track			1,511 mm		
Fuel capacity			64 L		
Tested capacity of stoddard solvent			59 L (91%)		
Seat type			Bucket, lever		
Position of front seats for test			Center		
Seat back angle			25.5°		
Steering wheel adjustment for test			Center		
OPTIONS					
x	Air conditioning		Traction control	x	Clock
	Tinted glass		All wheel drive		Roof rack
x	Power steering	x	Cruise control	x	Console
x	Power windows	x	Rear defroster	x	Driver air bag
x	Power door locks		Sun roof/T-top	x	Passenger air bag
	Power seat(s)	x	Tachometer	x	Front disc brakes
x	Power brakes	x	Tilt steering		Rear disc brakes
	Anti-lock brakes	x	AM/FM radio		Other
WEIGHTS (kg)		DELIVERED		FULLY LOADED	
Left front		411		437	
Right front		395		415	
Left rear		255		307	
Right rear		256		286	
TOTAL		1,317		1,445	
ATTITUDE (mm)		DELIVERED		FULLY LOADED	
Left front		687		676	
Right front		679		676	
Left rear		683		683	
Right rear		676		659	

Table 2. Vehicle description and statistics (continued).			
ATTITUDE (degrees)	DELIVERED	FULLY LOADED	TEST MODE
Driver	.8 down/front	.4 down/front	.7 down/front
Passenger	.2 down/front	.1 down/front	.2 down/front
Front	.7 up/left	.1 down/left	.6 down/left
Rear	.4 down/left	.1 down/left	.4 down/left
Cg (mm) measurements	DELIVERED	FULLY LOADED	TEST MODE
Behind front axle	1,054	1,115	1,093
Lateral	764	775	760

The test vehicle was prepared for testing following procedures outlined in FMVSS 214. A NHTSA supplied OSCAR was used to determine the position of the SID/HIII for testing. The OSCAR defines a three dimensional location of the H-point (hip point) of a dummy in relation to the driver door striker. This H-point measurement was used the morning of the test to place the dummy in the correct position.

The vehicle weight and four sill attitudes were measured in each of the three modes or configurations described in FMVSS 214. The first was the "as delivered" mode. This configuration consisted of the test vehicle as delivered from a dealership with its fuel tank filled to between 92 percent and 94 percent capacity with petroleum naphtha, a stoddard solvent (although actual for this test was only 91 percent). The second mode, cargo mode, consisted of the vehicle with one dummy placed in the driver seat and 45 kg of simulated cargo placed in the trunk along the vehicle centerline. The final mode was the "as tested" mode. This configuration consisted of the vehicle fully instrumented for testing. The four sill attitude measurements, vehicle weight distribution, and other measurements are presented in table 2. The vehicle attitudes up on the guidance rails were adjusted to within 0.5 degrees of the "test mode" measurements.

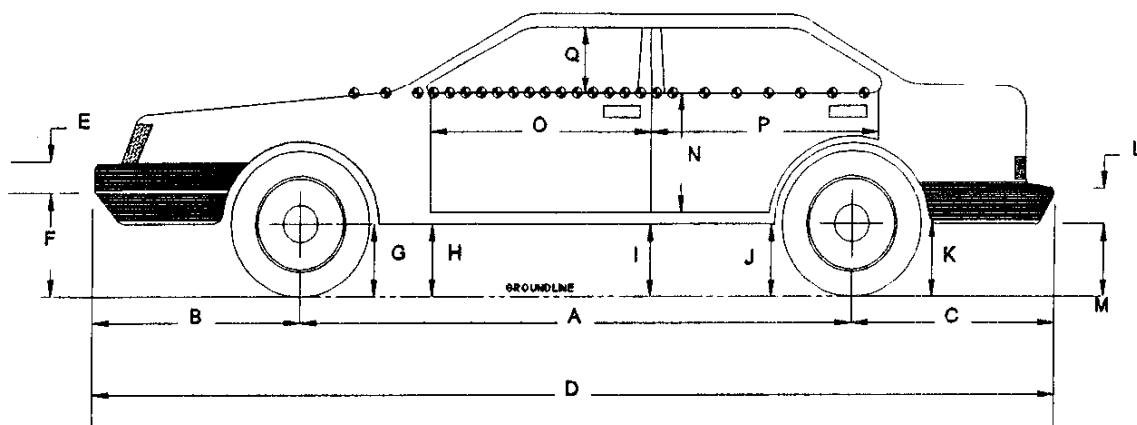
Included in the test mode configuration were the two side-impact carriages. The main monorail carriage rides down the main I-section monorail. The monorail carriage was bolted 200 mm forward of the vehicle's longitudinal cg. The main monorail carriage supports approximately 95 percent of the total vehicle weight. The monorail carriage includes a tow pin protruding out 200 mm rearward such that the tow cable pulled at the vehicle cg. The tow location allows for the least possible yaw to be induced by the tow system. The propulsion used was a gravity assist system. The FOIL utilizes a weight stack and a 6-to-1 mechanical advantage to accelerate the test vehicle. The total weight on

the weight stack was reduced to 2,310 kg to prevent the SID/HIII from tipping during acceleration. The rear carriage was bolted to the bumper of the test vehicle and rides along a 50-mm steel angle. The rear carriages typically supports 5 percent of the total vehicle weight. Each carriage was constructed from aluminum and remained fastened to the test vehicle throughout the test. To prevent significant interference by the carriages, the carriages were bolted to the test vehicle using small diameter hardware quality bolts. The bolts were to shear quickly in the event the carriages made substantial contact with a structural member.

The fuel tank useable capacity (from Honda of America) was 64.5 L. The fuel tank was filled with 58.7 L (91 percent of capacity) of petroleum naphtha (stoddard solvent) which has the same density as gasoline but is less volatile. The tank was filled to reflect a more realistic weight of a passenger vehicle on the road. The petroleum naphtha also provided a means to observe any fuel system component leakage after the test. The original lead-acid battery in a charged state remained in the engine compartment. The battery was disconnected to prevent frontal air bag deployment. The vehicle test weight, including the dummy, instrumentation, cameras, ballast, and stoddard solvent was 1,470 kg. The SID/HIII weight was 80 kg.

Target tape and circular targets were placed on the test vehicle in accordance with FMVSS 214. The 25-mm yellow and black target tape was placed along the struck side of the vehicle at five elevations. The elevations included the lower door sill, the mid-door height, occupant H-point height, top-door sill, and roof sill. The target tape was used to measure pre- and post-test side profile measurements to determine vehicle damage or crush. The FOIL used a 2.5 m long by 1.4 m high peg board placed along the driver (left) side of the vehicle to measure the vehicle profile. The board's position was referenced from two points directly across from the impact location on the right side of the vehicle. This was done to ensure that the reference location would not be severely damaged. The two points were chosen directly across from impact because the least amount of bowing occurs directly across from impact. It was necessary to position the board in the same position relative to the vehicle after the crash test to obtain accurate crush measurements. The pre- and post-test profile measurements are shown in figure 7 later in this report.

A list and sketches of the vehicle's physical parameters are shown in table 2 and figure 1, respectively. Figure 1 includes post-test damage measurements.



	PRE-TEST	POST-TEST	△CHANGE
A	2,718	2,477	-241
B	921	895	-26
C	1,022	1,035	13
D	4,655	4,407	-248
E	121	121	0
F*	416 / 406	413	7
G*	283 / 267	254	-13
H*	283 / 267	257	-10
I*	284 / 267	273	6
J1*	210 / 194	298	104
J2*	284 / 267	248	-19
K*	352 / 311	337	26
L	241	241	0
M*	335 / 337	337	0
N	635	660	25
O	1,102	965	-137
P	972	864	-108
Q	438	391	-47

* These measurements were taken in the "as delivered" and in the "as tested" configuration, respectively.

Figure 1. Vehicle physical parameters in millimeters.

INSTRUMENTED DUMMY

One SID/HIII, serial number 26, was placed in the driver seat of the Honda Accord. The SID/HIII was supplied by the NHTSA and was calibrated by a NHTSA-approved dummy calibration facility before shipment to the FOIL. The SID/HIII is a combination of the standard SID torso with the neck and head replaced with a HYBRID III dummy's neck and head. The neck bracket was removed from the SID and replaced with a new neck bracket specifically designed for the SID/HIII. This provided the necessary bolt pattern and alignment for a HYBRID III neck and head assembly. It was noted that the dummy's head had a slight twist about the neck. This may have been the result of the attachment between the neck and head, or between the neck and head assembly and the dummy's torso. Figure 2 is a sketch of the modifications made to the SID/HIII. The dummy was shipped with the necessary hardware for assembly. Tools at the FOIL were used to assemble the SID/HIII. Clothing (not including shoes) consisting of white thermal underwear was purchased and put on the dummy. Eighteen extension cables were supplied with the SID/HIII. The extensions allowed for installation of connectors necessary for attachment to the FOIL data acquisition system without removing the standard dummy connectors. The transducers within the dummy were of the half bridge type and therefore completion resistors were soldered into the connectors at the data acquisition system interface.

The morning of the test, the SID/HIII was positioned in the driver seat in accordance with FMVSS 214. The data acquired from the OSCAR was used to place the dummy H-point at the correct location. The driver seat was set in the center position with the back rest leaning back 25.5 degrees from the vertical position. Using FMVSS 214 as a guide and alignment tools supplied by the NHTSA, the SID/HIII's feet, legs, thighs, pelvis, torso, and head were positioned just before the test. Pertinent SID/HIII-to-interior longitudinal and lateral clearance measurements are shown in figure 3 and figure 4. Several different color chalks were put on the side surfaces of the dummy to determine the contact points between the dummy and the vehicle's interior, as shown in table 3 below.

Table 3. SID/HIII chalk colors.	
DUMMY PART	COLOR
Face	Blue
Top of head	Yellow
Left side of head	Green
Back of head	Red
Left hip	Red
Left shoulder	Blue

P572M HEAD/NECK/TORSO ASSEMBLY

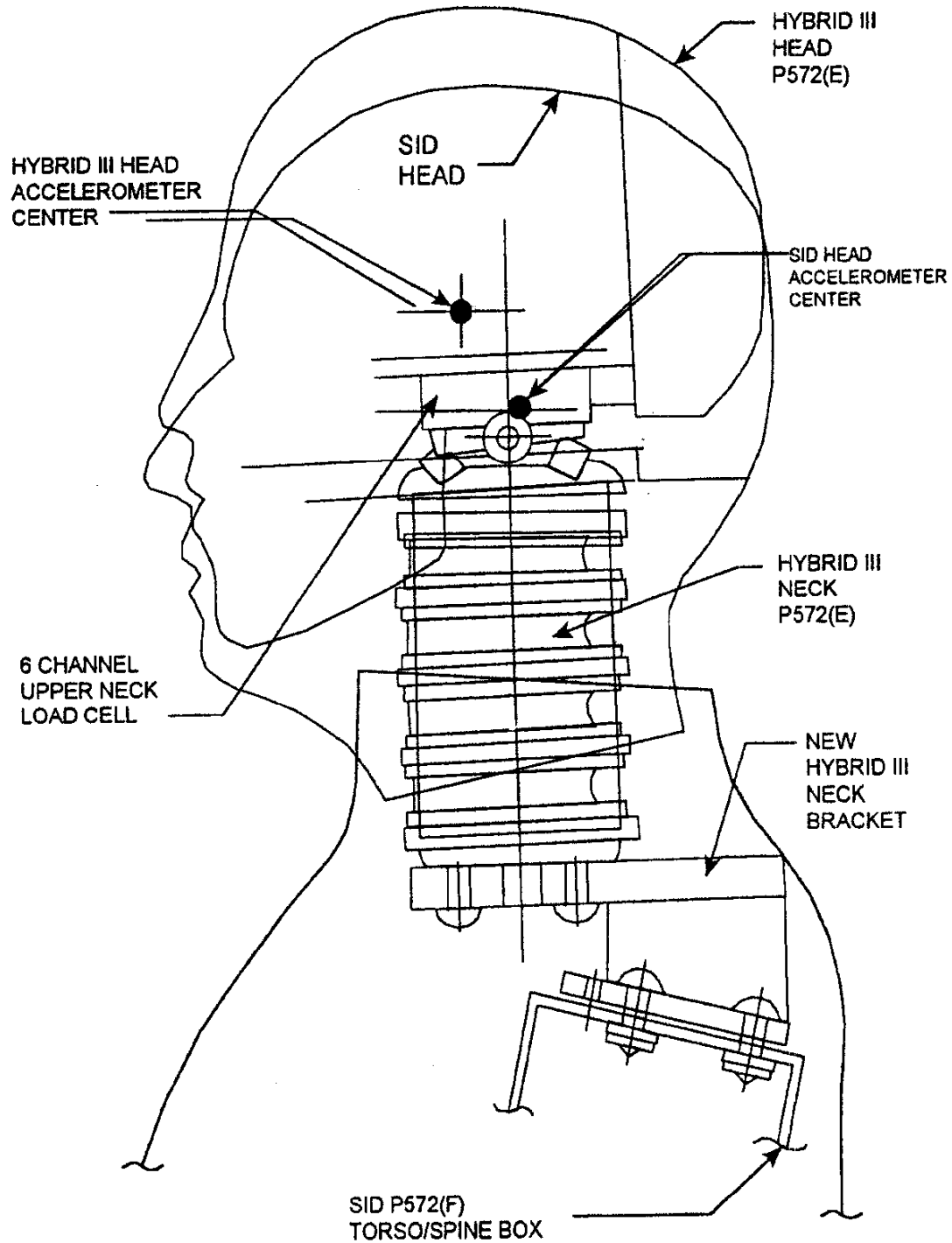
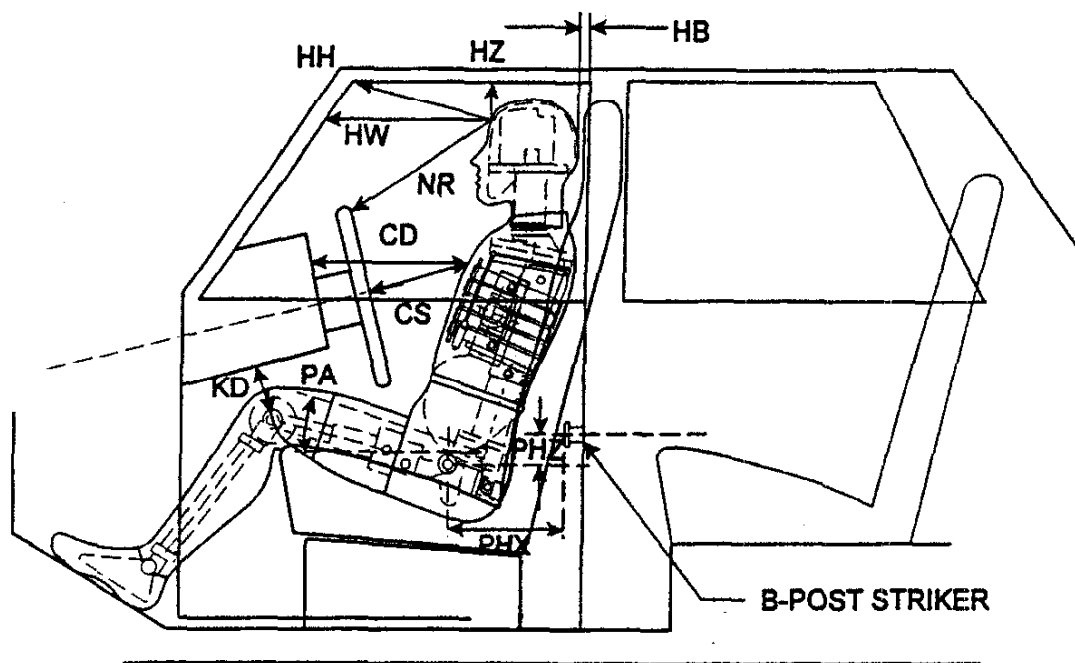


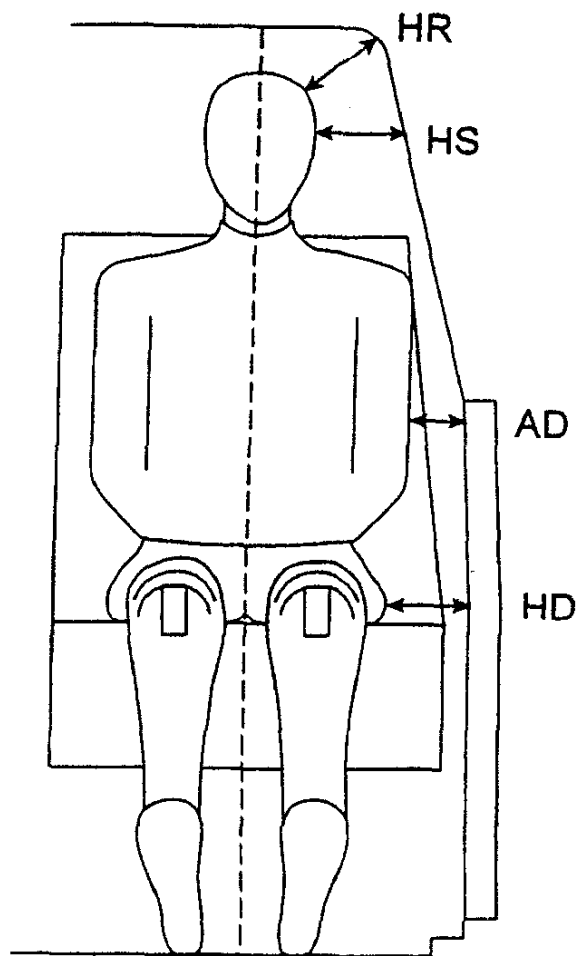
Figure 2. HYBRID III neck and head assembly on SID/HIII #26.



LEFT SIDE VIEW

MEASUREMENT (mm)	DRIVER SID/HIII ID# 26
HH	485
HW	636
HZ	205
HB	Head overlap B-pillar 75
NR	560
CD	616
CS	390
KDL(KDA degrees)	190 (24°)
KDR	210 (21.3°)
PA degrees	25°
PHX	245
PHZ	160

Figure 3. SID/HIII longitudinal clearance and position measurements.



MEASUREMENT (mm)	DRIVER SID/HIII ID# 26
HR	220
HS	330
AD	92
HD	152

Figure 4. SID/HIII lateral clearance and position measurements.

RIGID POLE

The FOIL instrumented 300K rigid pole was designed to measure vehicle frontal and side crush characteristics. The rigid pole was set up in the side-impact configuration. The rigid pole side-impact configuration consisted of four solid half-circle steel impact faces mounted to two load cells via two high-strength connecting rods per face (eight load cells total). The diameter of the pole impact faces was 255 mm. The load cells measured the forces exerted on the pole at each location. This provided insight into what structures on the vehicle produced the significant loads. The 300K rigid pole was mounted in line with the target impact location, aligned with the cg of the dummy's head.

A spike (e.g., sharpened welding rod) was affixed to one impact face to verify the impact location by physically puncturing the vehicle body. Figure 5 is a sketch of the FOIL 300K rigid pole (side-impact configuration).

INSTRUMENTATION

Electronic data from the crash test was recorded via two data acquisition systems, the FOIL umbilical cable system and the FOIL onboard data acquisition system (ODAS). A total of 39 channels of electronic data were recorded. The umbilical cable system recorded 13 data channels and the remaining 26 data channels were recorded by the ODAS system. In addition to electronic data, high-speed cameras were used to record the test on film which was analyzed to acquire pertinent test data. The following is a summary of the electronic data collected:

Vehicle instrumentation.

• Cg triaxial accelerometer (A_x, A_y, A_z)	3 channels
• Cg redundant accelerometer for A_y	1 channel
• Biaxial accelerometer, Engine (A_x, A_y)	2 channels
• Biaxial accelerometer, Trunk (A_x, A_y)	2 channels
• An accelerometer on driver seat (A_y)	1 channel
• Cg triaxial rate sensor (pitch, roll, yaw)	3 channels

SID/HIII instrumentation.

• Triaxial accelerometer dummy head (A_x, A_y, A_z)	3 channels
• Four dummy rib accelerometers (A_y)	4 channels
• Two dummy T12 spine accelerometers (A_y)	2 channels
• One dummy pelvis accelerometer (A_y)	1 channel
• Six dummy neck sensors ($F_x, F_y, F_z, M_x, M_y, M_z$)	6 channels

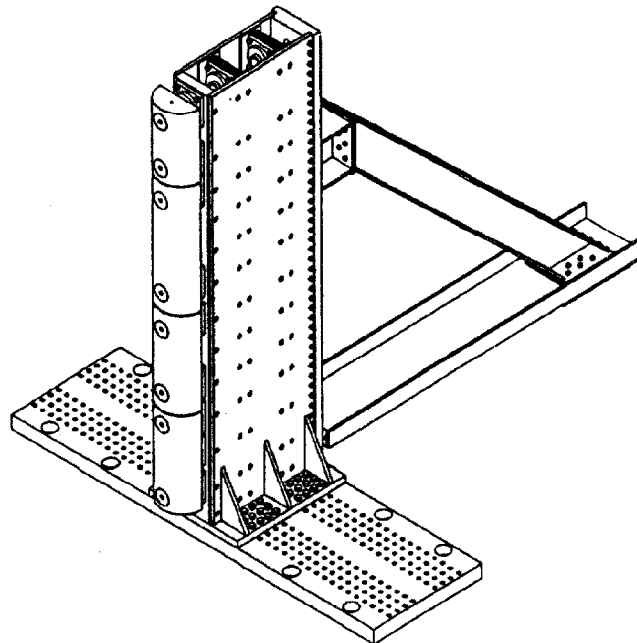
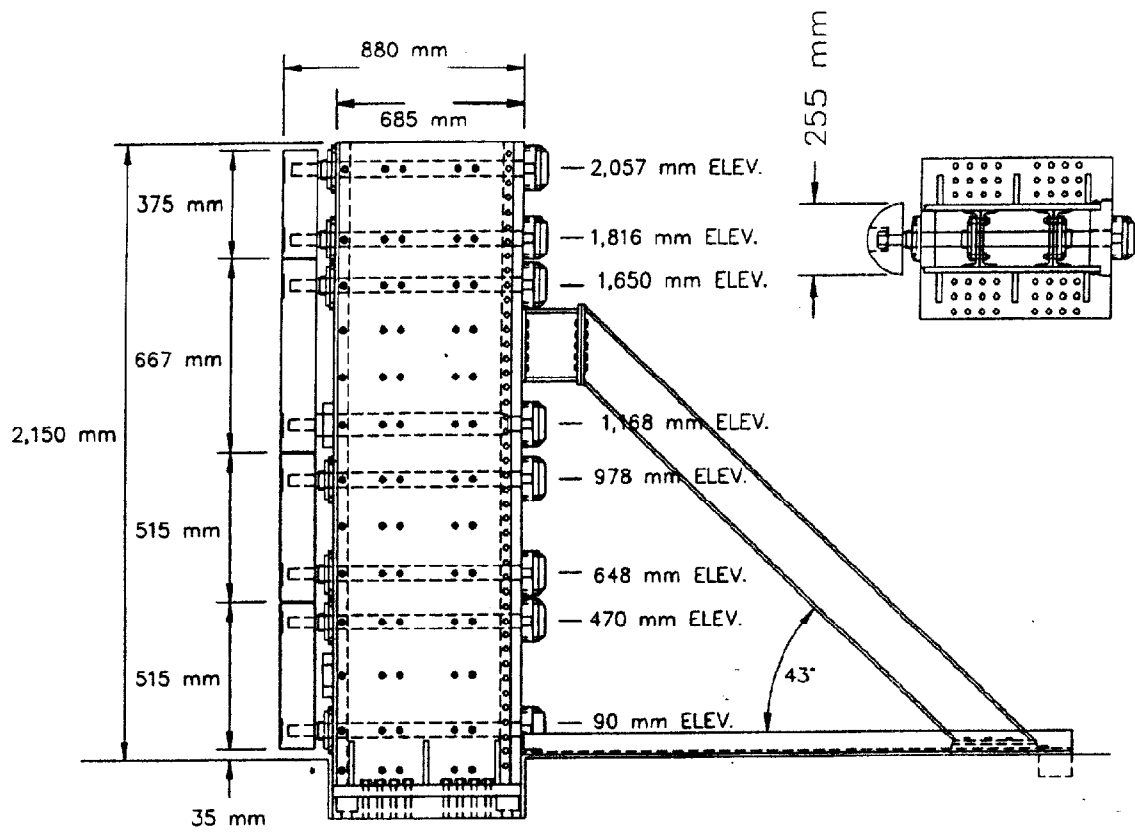


Figure 5. FOIL 300K instrumented rigid pole.

Rigid pole instrumentation.

- Eight rigid pole load cell channels (F_y) 8 channels

Miscellaneous.

- Impact and speed trap switches 2 channels
- 1 kHz timing signal for analog tape 1 channel

Table 4 provides specific channel assignments. The first 26 channels were ODAS channels including the 16 SID/HIII channels (shaded entries). The remaining channels were recorded via the umbilical cable tape recorder system.

Two methods for mounting accelerometers were used to affix the sensors to the test vehicle. The accelerometers were supplied with two small machine screws and a small 12-mm aluminum block. The first method used the accelerometer screws to mount the accelerometer to a small 25-mm², 6-mm thick steel plate, which was mounted to the vehicle using self-tapping sheet metal screws. This method was employed for the driver seat accelerometer. The second method used the aluminum block screwed to the small square-steel plate, which was welded to a larger, thicker plate. The larger plate was fastened to the vehicle using large self-tapping screws. This method was used for the accelerometers affixed to the engine block and in the trunk.

Onboard data acquisition system (ODAS)

The ODAS system collected 26 channels of data. The data was from cg, engine, driver seat, and trunk accelerometers, three rate transducers, and 16 SID/HIII channels. The output from the sensors were pre-filtered, digitally sampled, and digitally stored within the ODAS units mounted directly to the test vehicle inside the occupant compartment. The ODAS units are factory set with a 4000 Hz analog pre-filter and a digital sampling rate of 12,500 Hz.

Tape recorder-umbilical

The FOIL umbilical cable system utilizes a 90-m cable between the vehicle transducers, rigid pole load cells, or other sensors and a rack of 10 signal conditioning amplifiers. The output from the amplifiers was recorded on 25-mm magnetic tape via a Honeywell 5600E tape recorder. After the test, the tape was played back through anti-aliasing filters then input to a data translation analog-to-digital converter (ADC). The sample rate was set to 5,000 Hz. The system recorded outputs from the eight rigid pole load cells, two cg accelerometers, the monorail speed trap, and an impact contact switch to electronically mark first contact between the vehicle and rigid pole. The speed trap signals and the impact contact switch were not conditioned before being recorded.

The speed trap consisted of a single micro switch mounted to the monorail 4.2 m from the rigid pole. The wheels from the main side-impact carriage trip the switch as the vehicle passes over the speed trap. The distance between the two main carriage wheels is 1,015 mm.

Table 4. Summary of instrumentation.

ODAS III onboard data system			
Reference & Channel	Transducer	Max. range	Data description
1	Accelerometer	2000 g's	Head, X-axis
2	Accelerometer	2000 g's	Head, Y-axis
3	Accelerometer	2000 g's	Head, Z-axis
4	Accelerometer	2000 g's	Upper rib, Y-axis (P)
5	Accelerometer	2000 g's	Upper rib, Y-axis (R)
6	Accelerometer	2000 g's	Lower rib, Y-axis (P)
7	Accelerometer	2000 g's	Lower rib, Y-axis (R)
8	Accelerometer	2000 g's	Lower spine, Y-axis, T12 (P)
9	Accelerometer	2000 g's	Lower spine, Y-axis, T12 (R)
10	Accelerometer	2000 g's	Pelvis, Y-axis
11	Load cell	9000 N	Neck force, X-axis
12	Load cell	9000 N	Neck force, Y-axis
13	Load cell	9000 N	Neck force, Z-axis
14	Load cell	282 N·m	Neck moment, X moment
15	Load cell	282 N·m	Neck moment, Y moment
16	Accelerometer	100 g's	Z-axis, cg data
17	Accelerometer	100 g's	Y-axis, cg data
18	Rate transducer	500 deg/s	Pitch rate, cg
19	Rate transducer	500 deg/s	Roll rate, cg
20	Rate transducer	500 deg/s	Yaw rate, cg
21	Accelerometer	2000 g's	X-axis, engine block
22	Accelerometer	2000 g's	Y-axis, engine block
23	Accelerometer	2000 g's	Driver seat track

Table 4. Summary of instrumentation (continued).			
24	Load cell	340 N·m	Neck moment, Z moment
25	Accelerometer	2000 g's	X-axis, in trunk
26	Accelerometer	2000 g's	Y-axis, in trunk
Umbilical cable, tape recorder system.			
1	Accelerometer	100 g's	cg, X-axis
2	Accelerometer	100 g's	cg, Y-axis
3	Load Cell	111 kN	Bottom face, lower load cell
4	Load Cell	222 kN	Bottom face, upper load cell
5	Load Cell	222 kN	Lower middle face, lower load cell
6	Load Cell	222 kN	Lower middle face, upper load cell
7	Load Cell	222 kN	Upper middle face, lower load cell
8	Load Cell	222 kN	Upper middle face, upper load cell
9	Load Cell	111 kN	Top face, lower load cell
10	Load Cell	111 kN	Top face, upper load cell
11	Contact switch	1.5 Volts	Time of impact, T ₀
12	Micro switch	1.5 Volts	Mono-rail speed trap
13	Generator	1.5 Volts	1 kHz reference signal

High-speed photography

A total of seven high-speed cameras were used to record the side-impact collision. All high-speed cameras were loaded with Kodak color-daylight film 2253. The cameras operated at 500 frames per second and were positioned for best viewing of the contact between the Honda Accord and the 300K rigid pole. Three 35-mm still cameras and one 16-mm real-time telecine camera were used to document the pre- and post-crash environment. Table 5 lists each camera and lens used and the three dimensional location of the camera lens. The three dimensional coordinates were measured from the ground underneath the center of the semicircular impact faces of the rigid pole (origin) to the

camera lenses. The camera numbers in table 5 are shown in figure 6. The interior of the driver door was painted flat white for better onboard camera image quality.

Table 5. Camera configuration and placement.				
Camera Number	Type	Film speed (frames/s)	Lens (mm)	Orientation/ Location (m)
1	LOCAM II	500	100	90° to impact right side (15.5, 0, 0.84)
2	LOCAM II	500	45	90° to impact right side (16.2, 0, 1.3)
3	LOCAM II	500	40	45° oblique right side (6.7, 7.9, 0.86)
4	LOCAM II	500	50	45° left side (4.6, 8.4, 0.86)
5	LOCAM II	500	50	90° to impact left side (15.4, 0, 1.2)
6	LOCAM II	500	12.5	overhead, over rigid pole (0, 0, 6.0)
7	LOCAM II	500	5.7	on-board passenger window
8	BOLEX	24	zoom	documentary
9	CANON A-1 (prints)	still	zoom	documentary
10	CANON A-1 (slides)	still	zoom	documentary

Black and yellow circular targets, and black and yellow target tape 25-mm wide, were placed on the Honda Accord and rigid pole for film-data collection purposes. Circular targets and target tape were placed on the vehicle for certain vehicle measurements and for film analysis. The 25-mm tape was placed on the driver side of the vehicle at five levels or elevations referenced from the ground. The levels included:

- LEVEL 1 -- Axle centerline or lower door sill top height.
- LEVEL 2 -- Occupant H-point height.
- LEVEL 3 -- Mid-door height.
- LEVEL 4 -- Window sill height.
- LEVEL 5 -- Top of window height on roof rail.

In addition, target tape was placed vertically on the driver side of the vehicle coincident with the pole impact location. Target tape was also placed on top of the vehicle in the following locations:

- Along the longitudinal centerline the full length of the vehicle, excluding windows.
- Laterally across the roof perpendicular to the centerline tape and coincident with the rigid pole impact location.
- Laterally across the roof perpendicular to the centerline tape and coincident with the vehicle B-pillar.

Target tape was placed laterally on the front and rear bumpers in the YZ plane. Two vertical strips were placed on the rigid pole adjacent to and just rearward of the circular impact faces.

Black and yellow circular targets 100 mm in diameter were placed at various locations on the test vehicle for film data collection purposes. The targets were placed in the following locations:

- Driver door to denote the vehicle longitudinal cg.
- Driver door to denote the dummy H-point.
- The roof to denote the vehicle's longitudinal and lateral cg location.
- Two targets on the roof aligned with the vehicle longitudinal centerline 760 mm apart centered on the rigid pole centerline.
- Two targets aligned with the B-pillar centerline 610 mm apart centered on the vehicle's longitudinal centerline.
- Two targets on the hood aligned with the vehicle's longitudinal centerline 610 mm apart.
- Two targets on the trunk aligned with the vehicle's longitudinal centerline 255 mm apart.
- Two targets were placed on the front and back side of a vertical sheet metal stanchion fixed to the roof rearward of the B-pillar, centered on the longitudinal centerline and 610 mm apart.
- One target on top of the rigid pole's top semicircular impact face.
- Two targets on the front and rear bumper (YZ plane) 610 mm apart centered on the longitudinal centerline.

Figure 6 presents a side view of the test vehicle, showing the target tape locations. Figure 6 also contains an overhead sketch of the facility depicting the setup of the vehicle, rigid pole, test track, and the location of each high-speed camera. Positioned in each camera's view was at least one strobe light. The lights flashed when the vehicle struck the pole. This synchronized the film with the electronic data.

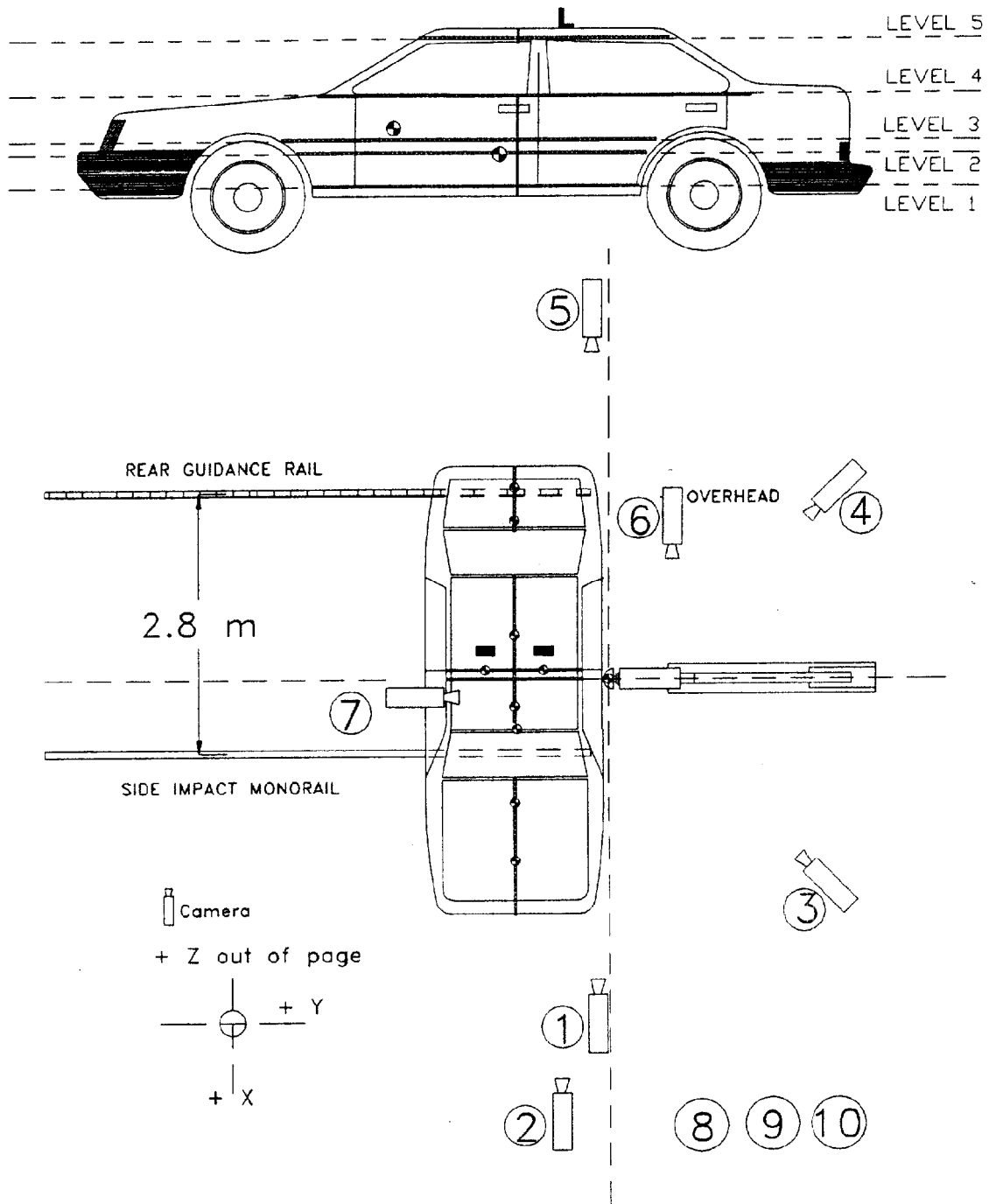


Figure 6. Camera locations and test setup.

DATA ANALYSIS

Two data acquisition systems, the ODAS system and the umbilical cable system, along with high-speed cameras were used to record the data during the side-impact crash test.

ODAS system. The data from the ODAS system included 16 channels of SID/HIII data, seven localized accelerometer channels, and three rate transducer channels. The data was filtered and digitally stored within the ODAS unit during the test. The filter was factory set at 4,000 Hz. The ADC sampling rate was factory set at 12,500 Hz. After the test, the data was down-loaded to a portable computer for analysis. The data was converted to the ASCII format, zero-bias removed, and digitally filtered at 1,650 Hz (Society of Automotive Engineers (SAE) class 1000). Rib, spine, and pelvic data were filtered a second time using a NHTSA-supplied FIR100 filter. The class-1000 data was input into a spreadsheet for plotting. The resultant head acceleration was calculated via a spreadsheet containing the data from the triaxial accelerometer inside the SID/HIII's head. The resultant acceleration data file was fed into a HIC algorithm to compute the HIC value for the crash test. The thoracic trauma index (TTI) was calculated from the FIR100 filtered rib and spine (T12) data. The following formula was used to compute the TTI:

$$TTI = [\text{Maximum}(4 \text{ rib channels}) + \text{Maximum}(\text{spine})] \div 2$$

Umbilical cable. Data collected via the umbilical cable tape recorder system was played back through an analog filter set at 1000 Hz. The signal was then input to a data translation ADC. The data included eight load cell channels, two accelerometer channels (located at the cg), an impact switch, and a monorail speed trap signal. The sample rate was set to 5,000 Hz. The digital data was converted to the ASCII format, zero-bias removed and digitally filtered to 1,650 Hz (SAE class 1000). The filtered data was input into a spreadsheet for plotting. The total force exerted on the rigid pole was computed by adding all eight load cell data signals and reading a peak from the combined force-time history.

Two square wave pulses from the lone monorail micro switch were recorded on analog tape during the crash test. The time between pulses was determined and the speed was calculated by dividing the wheel spacing (1,015 mm) by the time between micro switch pulses.

High-speed film. The high-speed 16-mm film was analyzed via an NAC 160-F film motion analysis system in conjunction with an IBM PC-AT. The overhead and one 90 degree camera were used to acquire pertinent test data. The analyzer reduced the test film frame by frame to cartesian coordinates which were input into a spreadsheet for analysis. Using the coordinate data and the known speed of the cameras, a displacement-time history was produced. Differentiation of the displacement-time history produced the initial vehicle speed. Data measurements included

initial vehicle impact speed, impact roll angle, impact yaw angle, and impact pitch angle.

RESULTS

The Honda Accord was placed on the FOIL side impact monorail with its longitudinal centerline perpendicular to the rigid pole centerline. The morning of the test the dummy was positioned in the driver seat using the H-point data and FMVSS 214. The SID/HIII's head cg was aligned with the rigid pole centerline. The dummy was restrained using the vehicle shoulder-lap belt restraining system. The rear third of the dummy's head overlapped the B-pillar. Just prior to testing, the following was noted: the emergency brake was placed in the engaged position, the head rests were positioned in the highest adjustment, the two front seats were aligned (mid-track position), the windows were down, the transmission was placed in neutral, and the key was placed in the "on" position. The Honda Accord passed over the monorail speed trap which measured a speed of 29.8 km/h. The impact yaw angle was 90° confirmed from high-speed film. Table 6 summarizes the test conditions and selected results.

Table 6. Summary of test conditions and results.	
FOIL test number	97S003
Date of test	May 28, 1997
Test vehicle	1995 Honda Accord LX, 4-door sedan
Vehicle weight	1,470 kg
Test article	FOIL instrumented 300K rigid pole
Temperature inside vehicle	24.4°C
Impact speed: speed trap	29.8 km/h
16-mm Film	29.9 km/h
Impact yaw angle	90°
Head impact point	Head struck B-pillar
Vehicle impact point (mm)	500 behind vehicle cg
Traffic accident data (TAD)	9-LP-7
Vehicle damage index (VDI)	09LPAN5
Head Injury Criteria (HIC)	
Limit	1000 g's

Table 6. Summary of test conditions and results (cont'd).	
Observed	667 g's
Start time	0.04712 s
Stop time	0.05488 s
Interval time	0.00776 s
Thoracic trauma data	
Limit (4-door)	85 g's
Peak rib acceleration (FIR100)	80.0 g's
T12 spine (FIR100)	49.0 g's
Thoracic Trauma Index (TTI)	64.5 g's

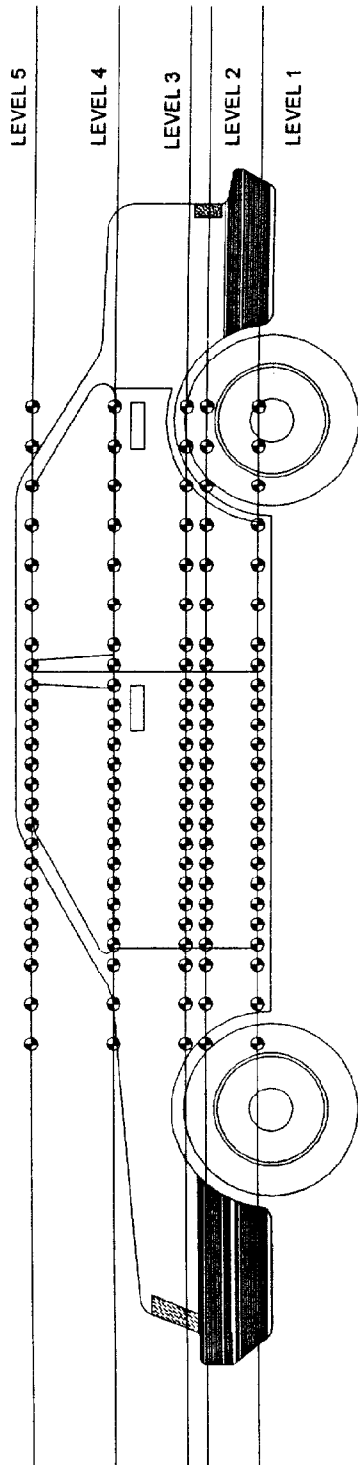
Vehicle response. The sharpened rod attached to the rigid pole punctured the vehicle 12.7 mm rearward of the vertical target tape centerline, denoting the intended target location. The puncture verified that the intended impact location was the first point of contact. Because the dummy was positioned such that it was partially shielded by the B-pillar, alignment of the rigid pole placed the pole in contact with most of the B-pillar. The B-pillar, front and rear doors collapsed, intruding into the occupant compartment. The pole rotated the driver seat counterclockwise (from overhead) and tipped the seat rearward 0.044 s after initial contact. Double integration of the cg acceleration-time history and the total rigid pole force-time history yielded a maximum dynamic intrusion of 700 mm. The driver seat collapsed and pinched the dummy's lower torso in the seat. The seat was pushed into and leaning behind the passenger seat. The impact location was 500 mm behind the vehicle cg. The lever induced a yaw into the vehicle after the peak load was reached. Integration of the yaw rate transducer positioned under the dash panel on the floor tunnel at the longitudinal and lateral cg produced a maximum yaw angle of 45 degrees which occurred at 0.720 s. The vehicle rebounded away from the pole as it continued to yaw counterclockwise (as seen from above). Contact between the main carriage and monorail impeded the vehicle motion, limiting the yaw and rebound. The four-door latches remained latched during the collision. No evidence of fuel leakage or fuel system component damage was observed. The driver air bag did not deploy during the test. As the pole penetrated the occupant compartment, the trunk release and gas filler-cap door cable were pulled, opening the trunk and filler-cap door. The peak cg acceleration was determined to be 17.2 g's (248 kN) and occurred 0.0378 s after impact. Table 7 lists the vehicle accelerometers and their three dimensional coordinate location referenced from the right front wheel hub. The right front wheel hub was 290 mm above ground (not on guidance rails). Included in the table are peak accelerations from each accelerometer (SAE class 60 data).

Table 7. Vehicle sensor locations and peak measurements.				
Sensor	X (mm)	Y (mm)	Z (mm)	Peak g's SAE Class 60
Cg accelerometer A_x	-1,005	710	125	-2.3
Cg accelerometer A_y	-1,005	710	125	-17.2
Cg redundant A_z	-1,005	710	125	6.5
Cg redundant A_y	-1,005	710	125	-14.7
Engine block A_x	180	880	485	-3.2
Engine block A_y	180	880	485	-7.4
Trunk A_x	-3,490	830	25	4.9
Trunk A_y	-3,490	830	25	-14.5
Driver seat A_y	-1,500	135	25	-64.4

After the test, damage profile measurements were taken using two techniques. Table 8 summarizes the damage profile distance (DPD) technique. Figure 7 depicts the driver-side profile measurements before and after the test. The measurements were made using a reference line parallel to the driver side of the vehicle. The parallel line was drawn a certain distance from and perpendicular to a line formed by the passenger side sill across from the impact location. This allowed the same reference line to be drawn after the test to measure the post-test measurements. The measurements were made in 75-mm and 150-mm increments forward and aft of the impact point. After the test, measurements were taken at the same points forward and aft rather than measuring at the same increments. From the figure, the maximum static deflection recorded was 549 mm at mid-door height along the vertical impact target tape.

Data plots of the data from transducers mounted to the test vehicle are presented in appendix A. Photographs taken from high-speed film during impact and photographs of the pre- and post-test environment are presented in appendix C.

Table 8. DPD crush measurements (mm).										
L	D	Max	LF	C1	C2	C3	C4	C5	C6	LR
1,830	-340	541	-1,020	0	148	341	511	182	0	810
L = total length of crush. D = distance from vehicle cg to mid-point of L Max = maximum crush LF, LR = distance from impact point to points forward and rearward where no damage was observed. C1-6 = incremental crush measurements along L, equally spaced.										



Level 1 - Sill height Level 2 - Occupant H-point Level 3 - Mid-door Level 4 - Window sill Level 5 - Window top

LEVEL	HEIGHT	Distance from impact point (mm).														
		1,067	-914	-838	-762	-686	-610	-533	-457	-381	-305	-229	-152	-76		
1	273	PRE	835	841	848	848	845	848	848	851	845	848	851	848		
	318	POST	972	1,010	1,022	1,041	1,080	1,092	1,099	1,124	1,149	1,213	1,257	1,311		
		CRUSH	137	169	174	193	232	247	251	276	298	336	365	406	463	
2	457	PRE	794	797	803	810	810	810	810	811	810	806	803	806		
	495	POST	914	972	991	1,016	1,043	1,092	1,105	1,130	1,168	1,226	1,257	1,311		
		CRUSH	120	175	188	204	233	282	295	319	358	394	420	454	505	
3	584	PRE	794	797	803	810	810	810	810	811	810	806	803	810		
	614	POST	914	967	997	1,019	1,067	1,099	1,099	1,124	1,143	1,232	1,280	1,321		
		CRUSH	120	170	194	209	257	289	289	313	333	377	426	477	511	
4	883	PRE	851	848	857	854	854	857	864	864	870	867	867	860		
	927	POST	959	967	991	1,010	1,080	1,118	1,118	1,156	1,181	1,207	1,251	1,283	1,321	
		CRUSH	106	119	134	156	226	261	254	292	311	340	384	416	461	
5	1,340	PRE									1,140	1,130	1,133	1,137	1,133	
	1,422	POST									1,257	1,283	1,308	1,340	1,372	
		CRUSH									117	153	175	203	239	

All units of measurement are in mm.

Figure 7. Vehicle profile measurements, test 97S003.

LEVEL	HEIGHT	Distance from impact point (mm).									
		0	76	152	229	381	533				
1	273	PRE	845	860	860	854	886				
	318	POST	1,334	1,314	1,257	686	1,067	1,022			
		CRUSH	489	454	397	164	213	136			
2	457	PRE	803	803	803	803	810	813			
	495	POST	1,334	1,334	1,283	1,207	1,099	997			
		CRUSH	531	531	480	404	289	184			
3	584	PRE	797	800	800	800	803	810			
	614	POST	1,346	1,327	1,283	1,213	1,105	1,010			
		CRUSH	549	527	483	413	302	200			
4	883	PRE	865	867	867	873	879	891			
	927	POST	1,356	1,397	1,346	1,308	1,219	1,124			
		CRUSH	491	530	479	435	340	233			
5	1,340	PRE	1,111	1,133	1,137	1,140	1,140	1,140			
	1,422	POST	1,422	1,416	1,378	1,353	1,276	1,238			
		CRUSH	311	283	241	213	156	98			
All units of measurement are in mm.											

Figure 7. Vehicle profile measurements (continued).

Occupant response. The SID/HIII remained vertical in the driver seat with only minor vibration induced by the tow and guidance system. The first contact occurred 0.024 s after impact and was between the door and the SID/HIII's shoulder region. The back third of the SID/HIII's head struck the B-pillar at 0.050 s. This prevented significant head protrusion from the window. The head rotated about the neck, and the face made slight contact with the pole at 0.064 s. The neck Z-moment load cell verified this event. The rotation away from the pole and energy absorption of the B-pillar did not allow significant contact between the SID/HIII's head and the rigid pole. After the test, no physical damage to the SID/HIII was observed. The dummy was wedged between the door and the emergency brake handle. The dummy's final position was slumped over, leaning toward the passenger seat while his lower torso remained wedged in the driver seat. Green and red chalk was found on the upper seat belt anchor and B-pillar indicating significant contact by the left side and rear of the SID/HIII's head. A small amount of yellow chalk was found on the rigid pole, verifying contact between the dummy's head and the pole. Blue chalk was also found on the pole, indicating contact from the dummy's shoulder. After review of the test film, it was determined the chalk was a result of splatter and not from direct contact between the shoulder and rigid pole. Blue chalk from the dummy's side was on the B-pillar and door as expected. Red chalk from the dummy's femur and leg was found on the driver door.

The rib and spine produced a TTI of 64.5 g's. This is below the four-door sedan limit of 85 g's specified in the FMVSS 214. The three head accelerometers produced a HIC value of 667 g's. This value is below the 1000 g's required in the proposed FMVSS 201 amendment. Table 9 summarizes the data collected from the SID/HIII.

Table 9. Summary of SID/HIII data.		
Recorded Data	Maximum positive	Maximum negative
Head X-axis acceleration(g's)	9.9	-20.6
Head Y-axis acceleration (g's)	8.8	-111.2
Head Z-axis acceleration (g's)	8.4	-32.4
X-axis neck force load cell (N)	103.6	-352.3
Y-axis neck force load cell (N)	302.7	-1003.8
Z-axis neck force loadcell (N)	383.4	-1280.9
X-axis neck moment load cell (1000 mm·N)	21.7	-84.3
Y-axis neck moment load cell (1000 mm·N)	21.1	-21.5

Table 9. Summary of SID/HIII data (continued).		
Z-axis neck moment load cell (1000 mm·N)	14.8	-29.4
Left upper rib acceleration (P)	14.0	-77.7
Left upper rib acceleration (R)	14.3	-80.0
Left lower rib acceleration (P)	12.0	-70.8
Left lower rib acceleration (R)	11.5	-74.2
Spine T12 Y acceleration (P)	17.6	-49.0
Spine T12 Y acceleration (R)	17.6	-48.5
Pelvis Y acceleration	14.6	-41.6
Head and neck load data is SAE class 1000. Shaded area data is SAE class 600 (neck moment data). Remaining data obtained from FIR100 filter output.		

The values from the head accelerometers and the neck load cells were taken from class 1000 data (neck moments, class 600) while the remainder was from data filtered using a FIR100 filter. Data plots from the SID/HIII transducers are presented in appendix B. All data plots are of class 1000 data.

Rigid pole. The load cells measured eight separate forces on the rigid pole. The total load from summing the eight load cells was 97,800 N. The significant loads were contributed by the roof-rail, floor-sill, and middle-point of the driver door. Table 10 summarizes the load cell data (SAE class 60). Data plots from the rigid pole load cells are presented in appendix D.

Table 10. Summary of rigid pole data.		
Load cell/height (mm)	Peak force (1000 N)	Time (ms)
Top face	-4.4	63.6
Upper load cell/2,057	-2.3	63.4
Lower load cell/1,816	-1.3	48.0
Middle-upper face	-10.7	67.8
Upper load cell/1,650	-5.7	66.8
Lower load cell/1,168	-5.1	67.4
Middle-lower face	-49.0	8.8
Upper load cell/978	-15.2	9.0
Lower load cell/648	-35.6	8.6

Table 10. Summary of rigid pole data (cont'd).		
Bottom face	-48.7	57.0
Upper load cell/470	-30.6	52.8
Lower load cell/90	-20.0	76.8
Total, rigid pole	-97.8	52.6

CONCLUSIONS AND OBSERVATIONS

Visual inspection of the Honda Accord after the collision produced immediate conclusions. The speed was within reasonable tolerance and the vehicle struck the rigid pole at the intended impact location.

Fuel system and door latch integrity were not breached by the broadside collision with the FOIL instrumented rigid pole (narrow-fixed object). Red, green, and yellow chalk on the B-pillar indicated significant contact between the B-pillar and the dummy's head (side, rear, and top). This contact caused the dummy to rotate away from the rigid pole, thus lowering contact with the rigid pole. The HIC value was below expected results for a broadside collision with a narrow object aligned with dummy's head cg. The test did not yield adequate results to show that a dynamic side-impact protection system would be of significant improvement. The injury criteria are below current safety standards without an air bag system present.

Further testing is needed to determine the repeatability of the laboratory test procedures and the results.

APPENDIX A. DATA PLOTS FROM VEHICLE ACCELEROMETERS.

Test No. 97S003

X-axis, acceleration vs. time cg data

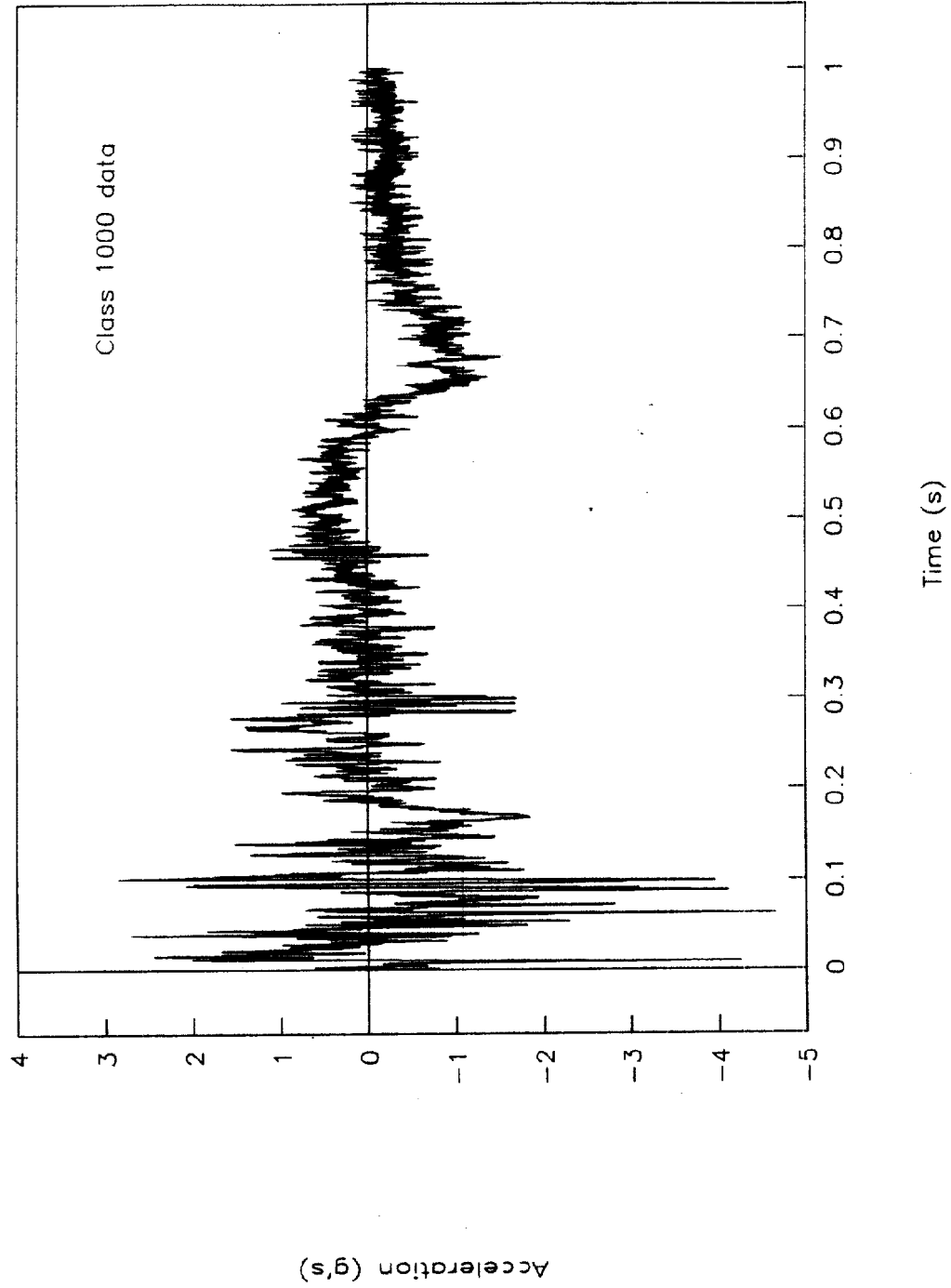


Figure 8. Acceleration vs. time, cg X-axis, test 97S003.

Test No. 97S003

Y-axis, acceleration vs. time cg data

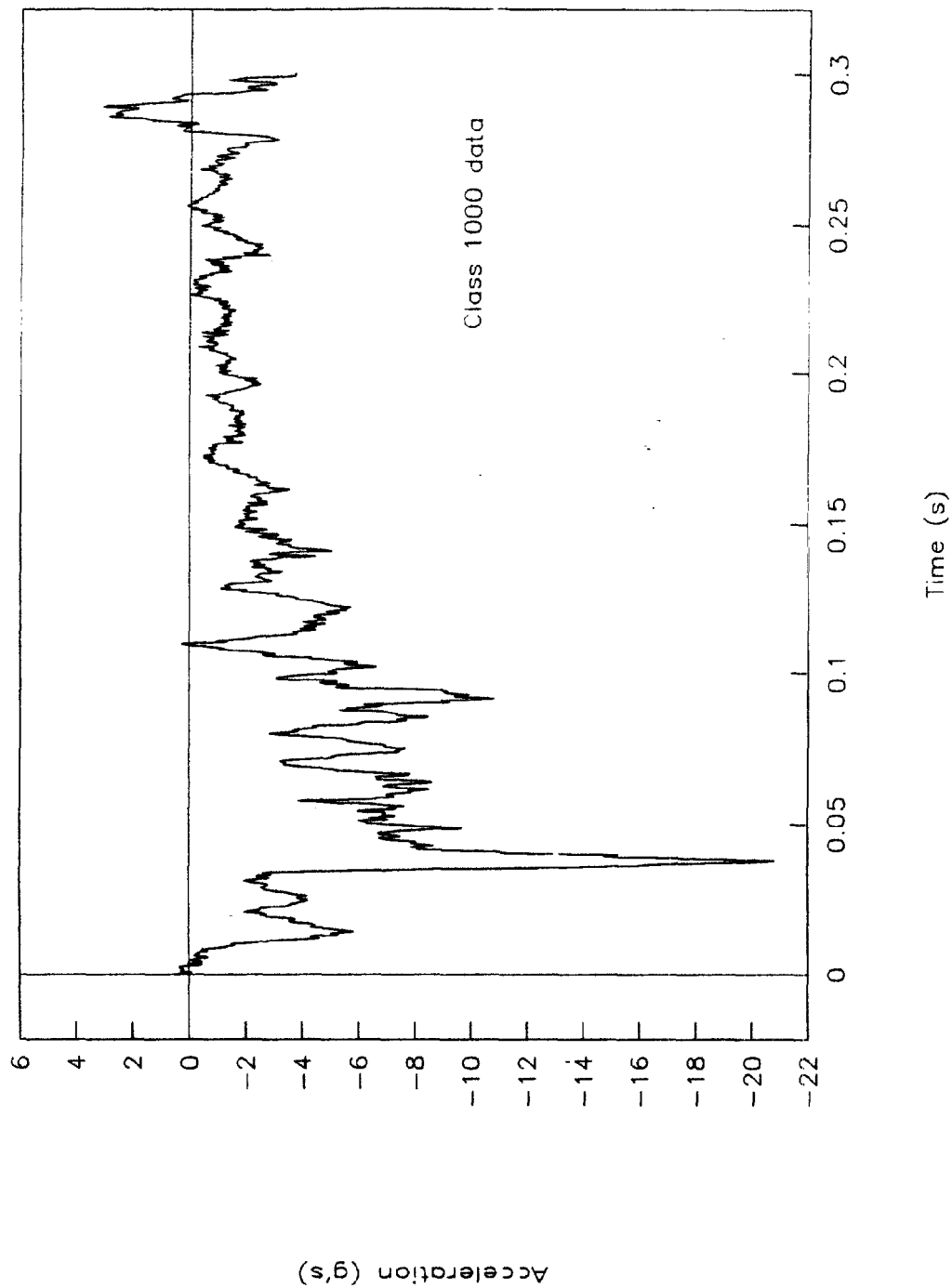


Figure 9. Acceleration vs. time, cg Y-axis, test 97S003.

Test No. 97S003
Z-axis acceleration vs. time, cg data

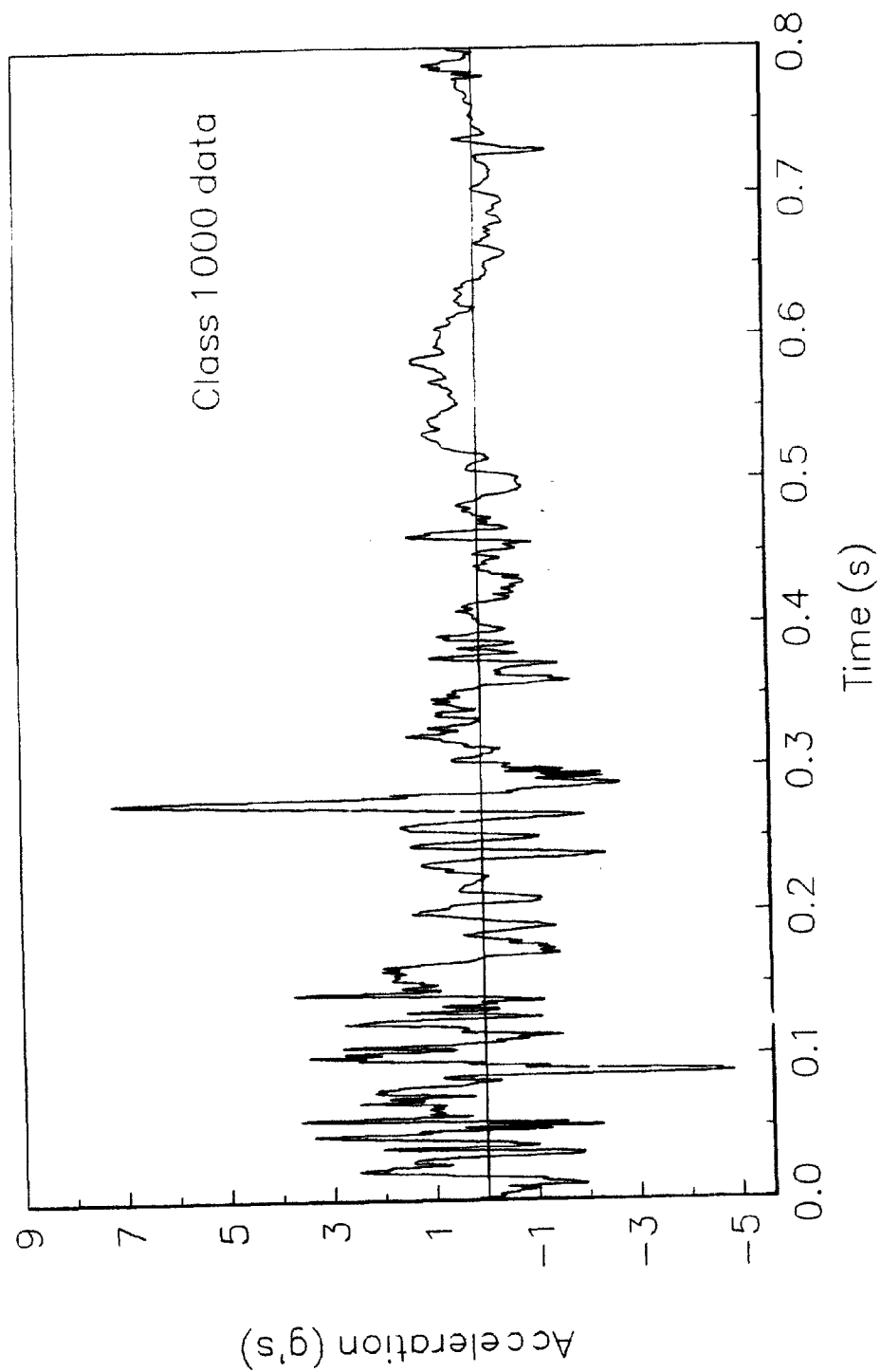


Figure 10. Acceleration vs. time, cg Z-axis, test 97S003.

Test No. 97S003
Redundant Y-axis cg data

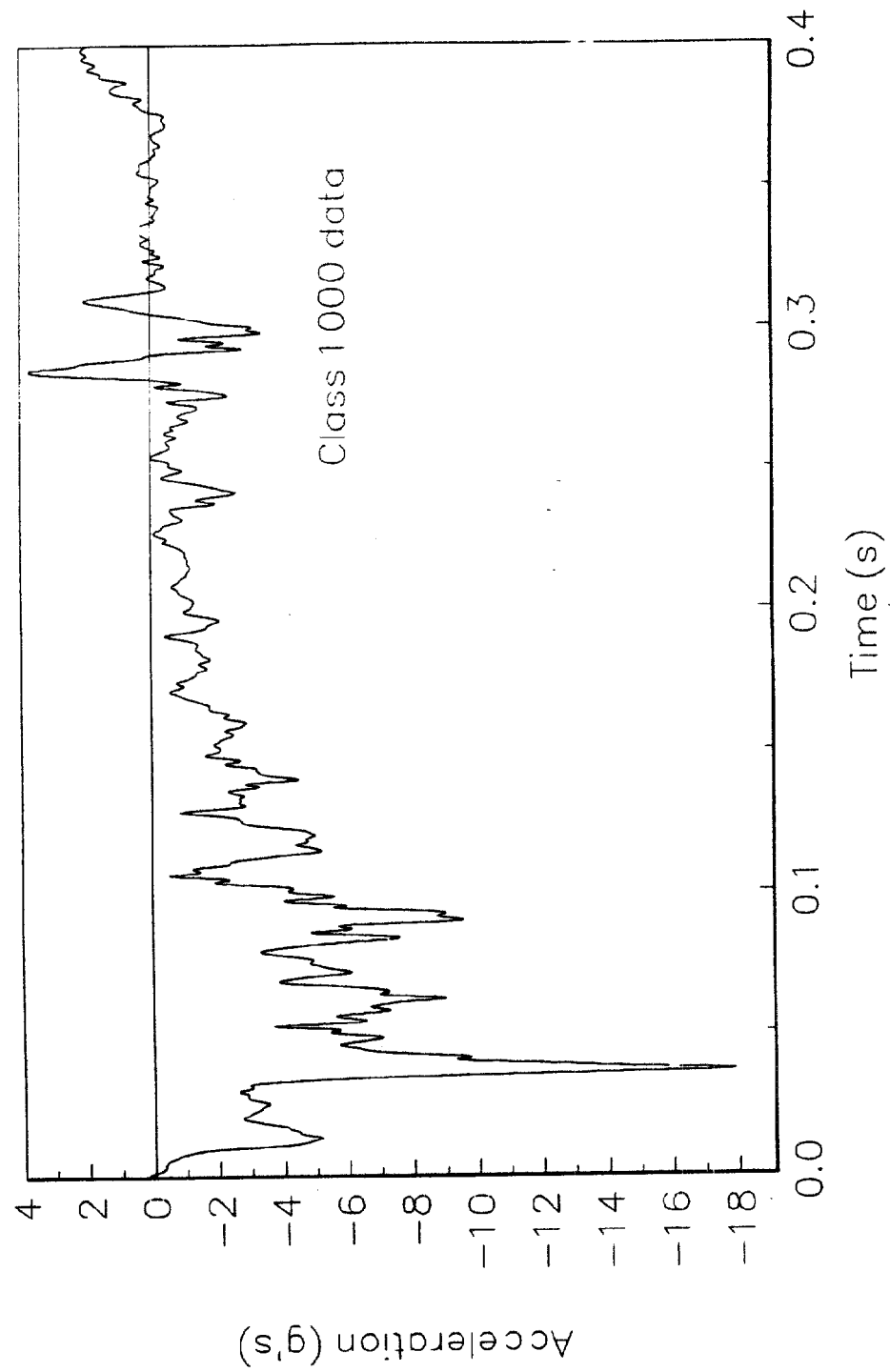


Figure 11. Acceleration vs. time, redundant Y-axis cg, test 97S003.

Test No. 97S003
Y-axis driver seat track

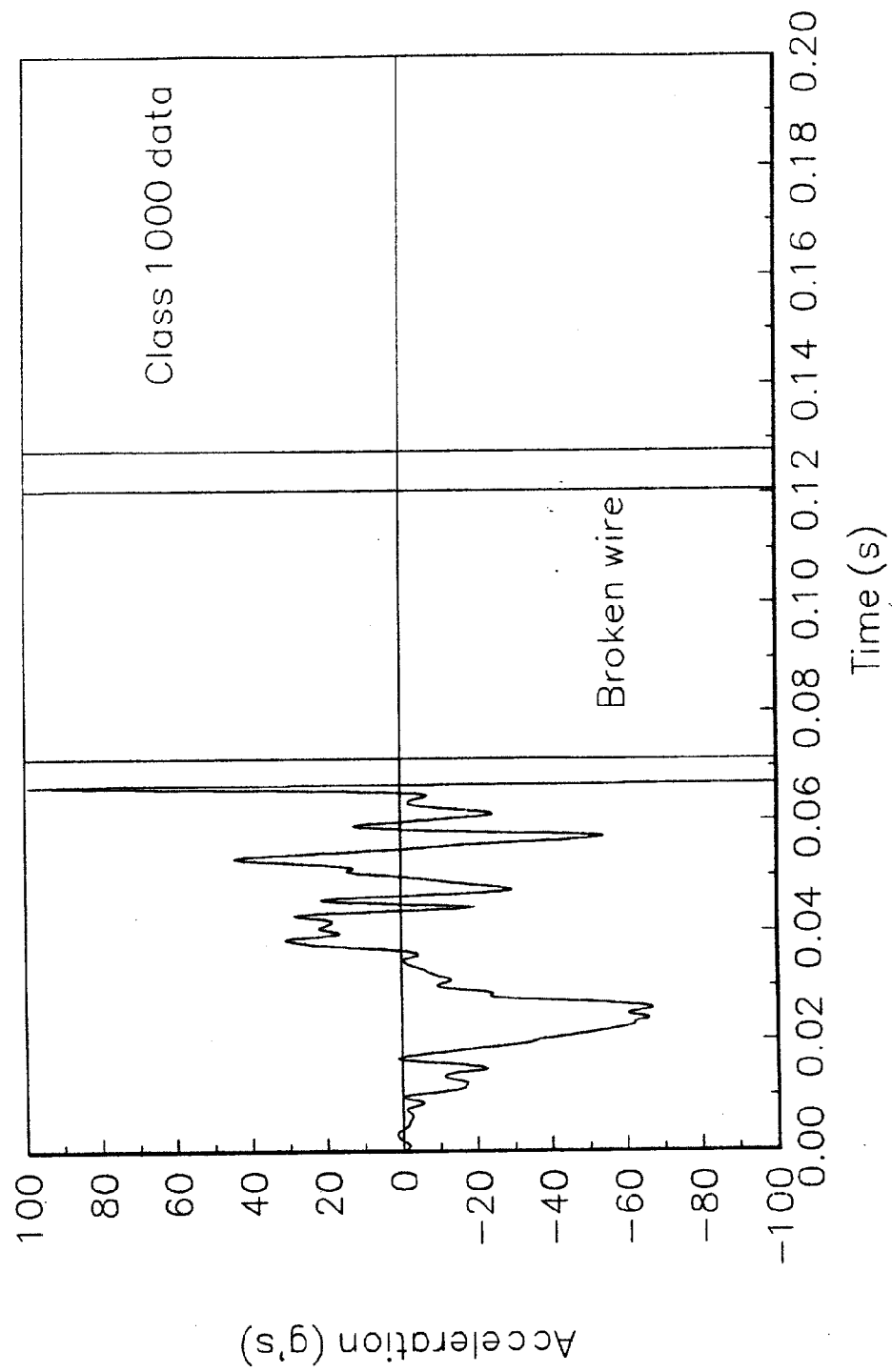


Figure 12. Acceleration vs. time, Y-axis driver seat track, test 97S003.

Test No. 97S003
X-axis engine block

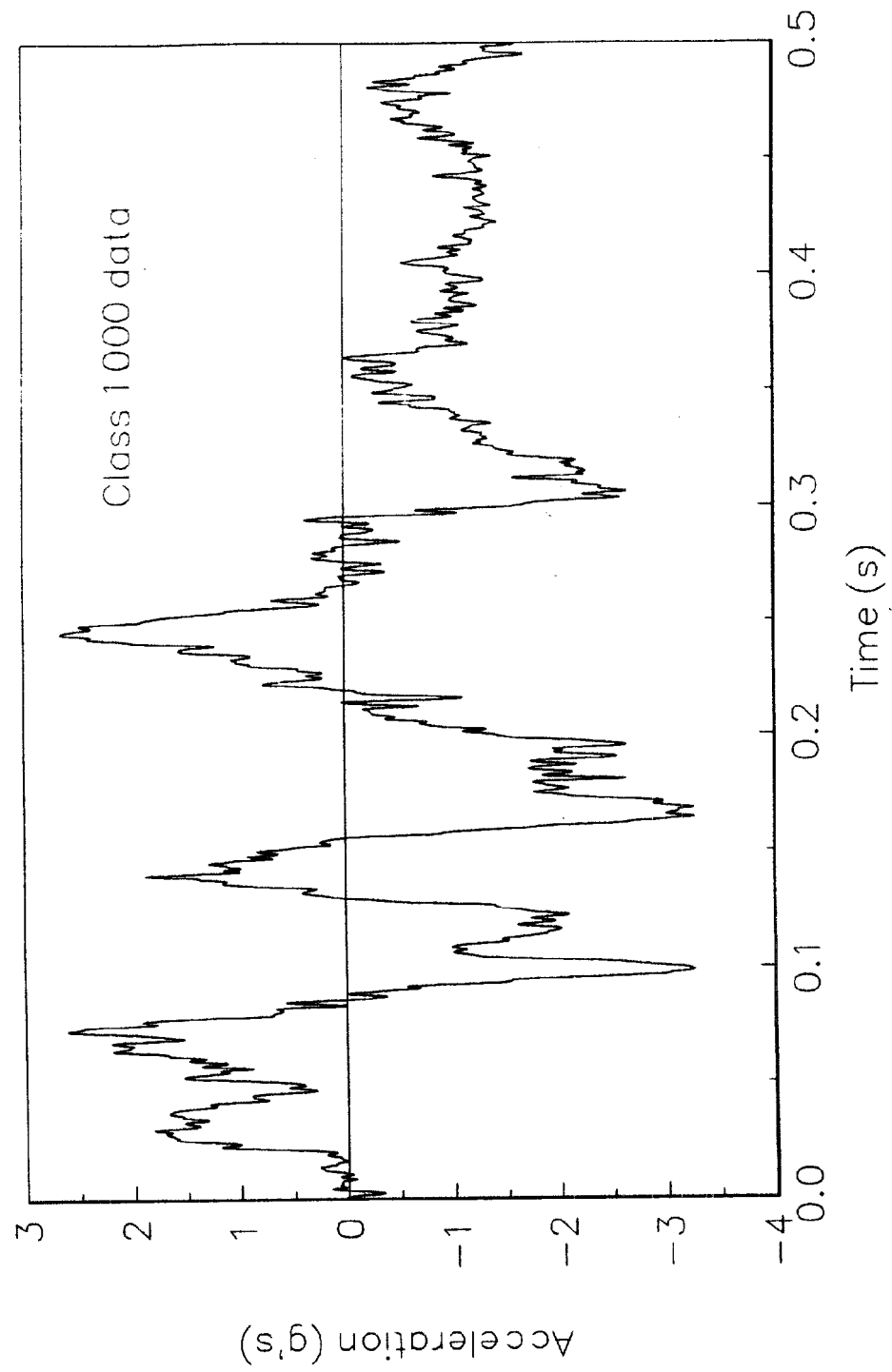


Figure 13. Acceleration vs. time, X-axis engine block, test 97S003.

Test No. 97S003
Y-axis engine block

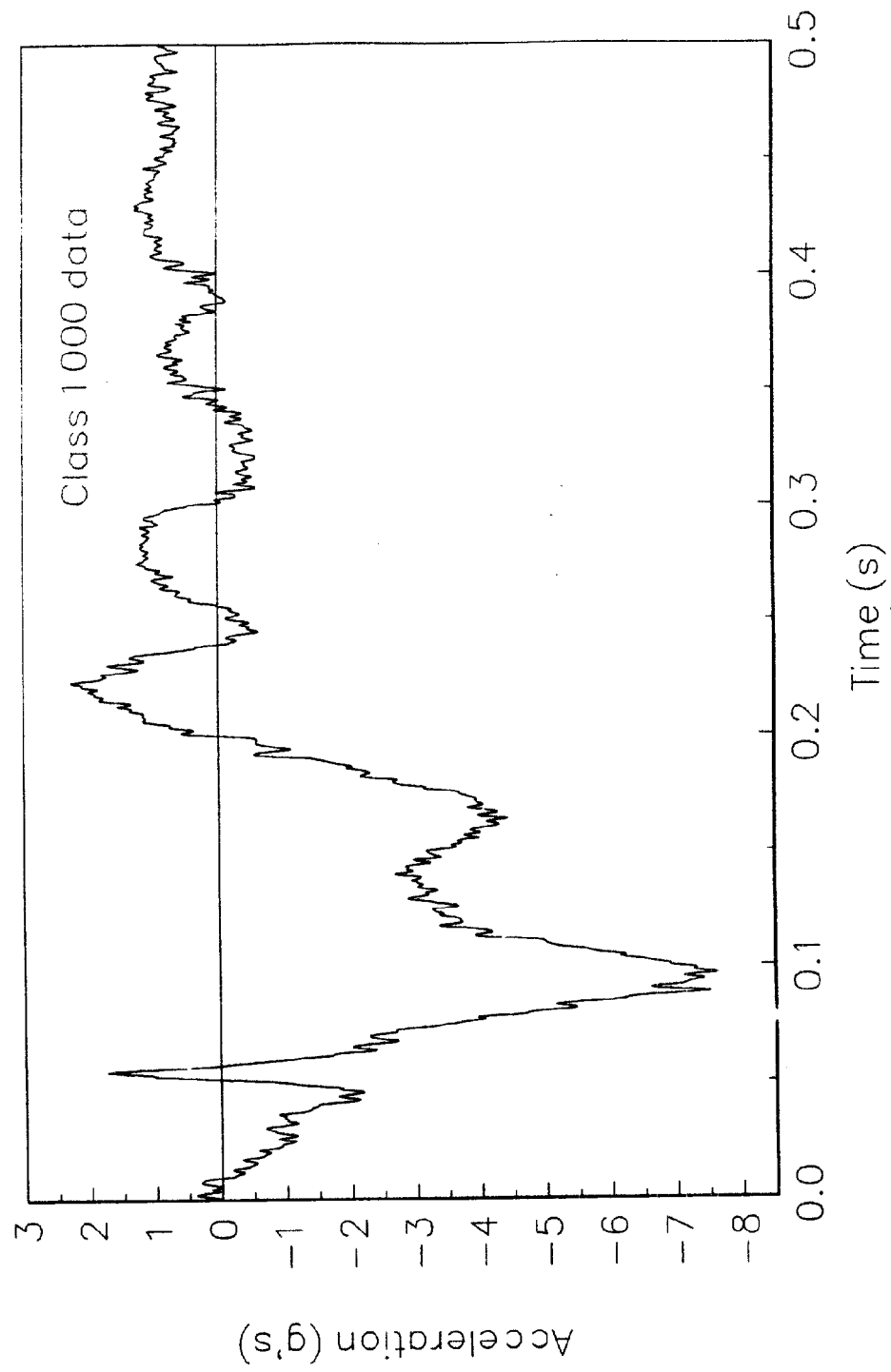


Figure 14. Acceleration vs. time, Y-axis engine block, test 97S003.

Test No. 97S003
X-axis trunk

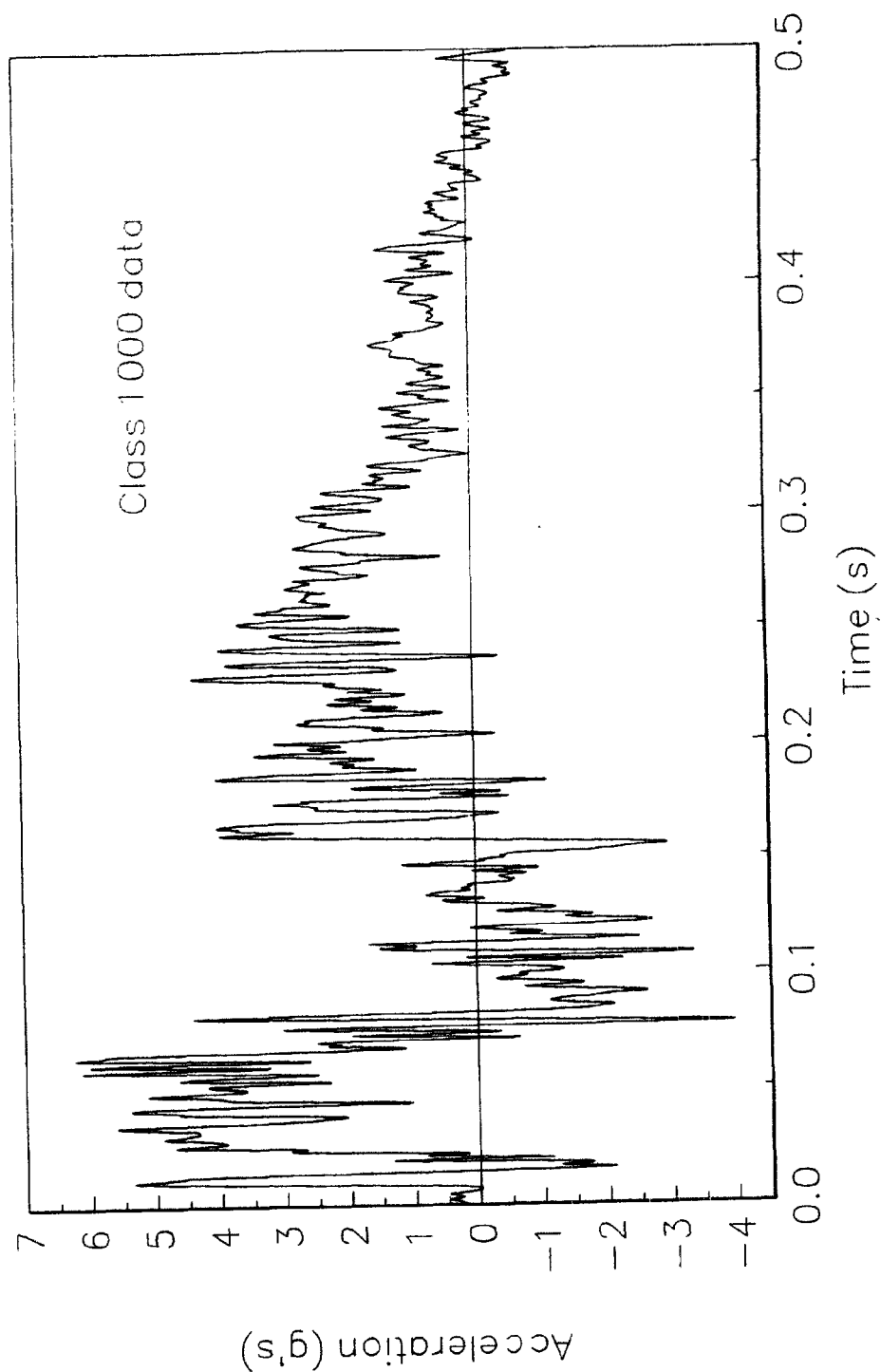


Figure 15. Acceleration vs. time, X-axis trunk, test 97S003.

Test No. 97S003
Y-axis trunk

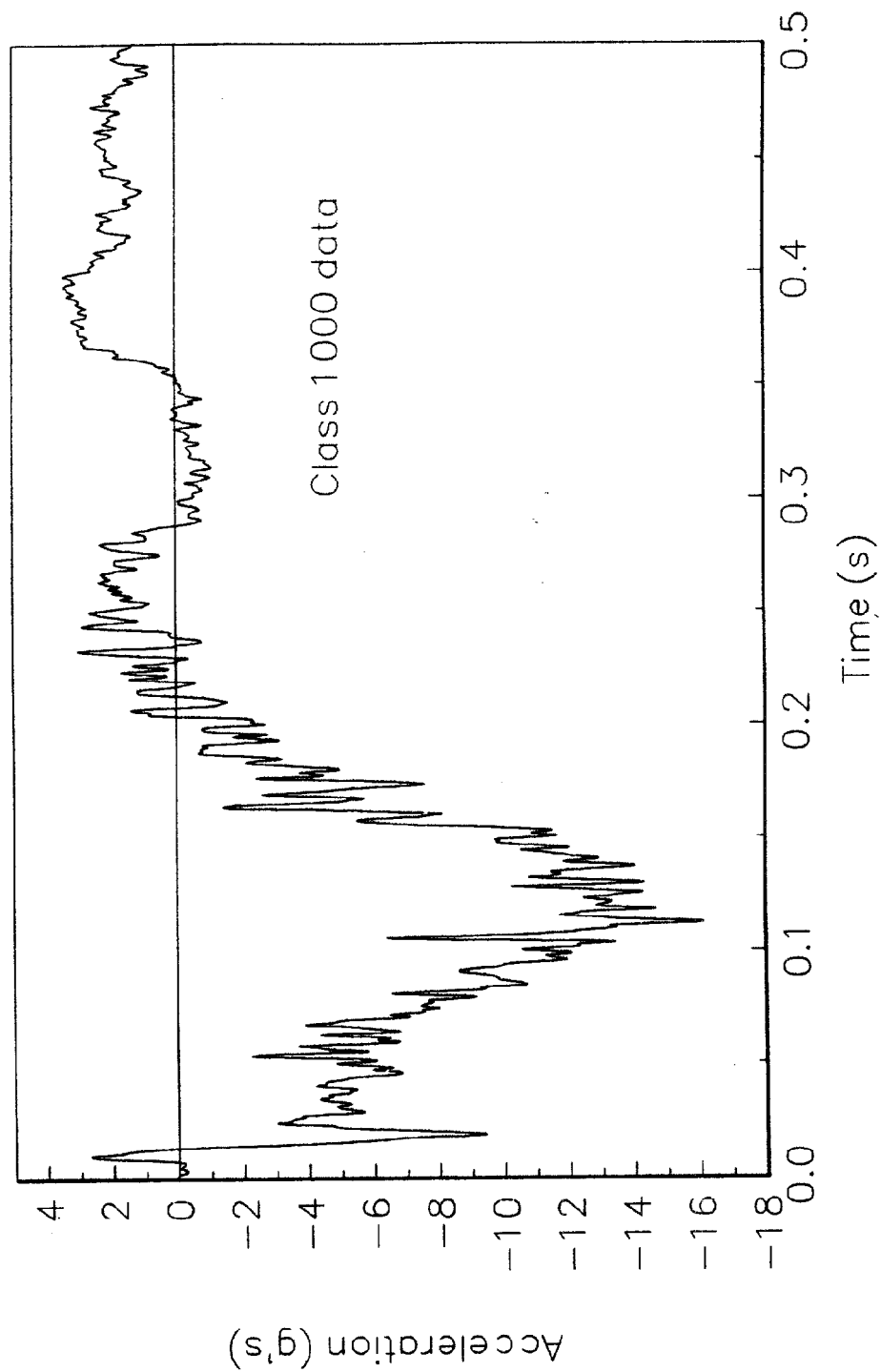


Figure 16. Acceleration vs. time, Y-axis trunk, test 97S003.

Test No. 97S003
Pitch rate and angle vs. time

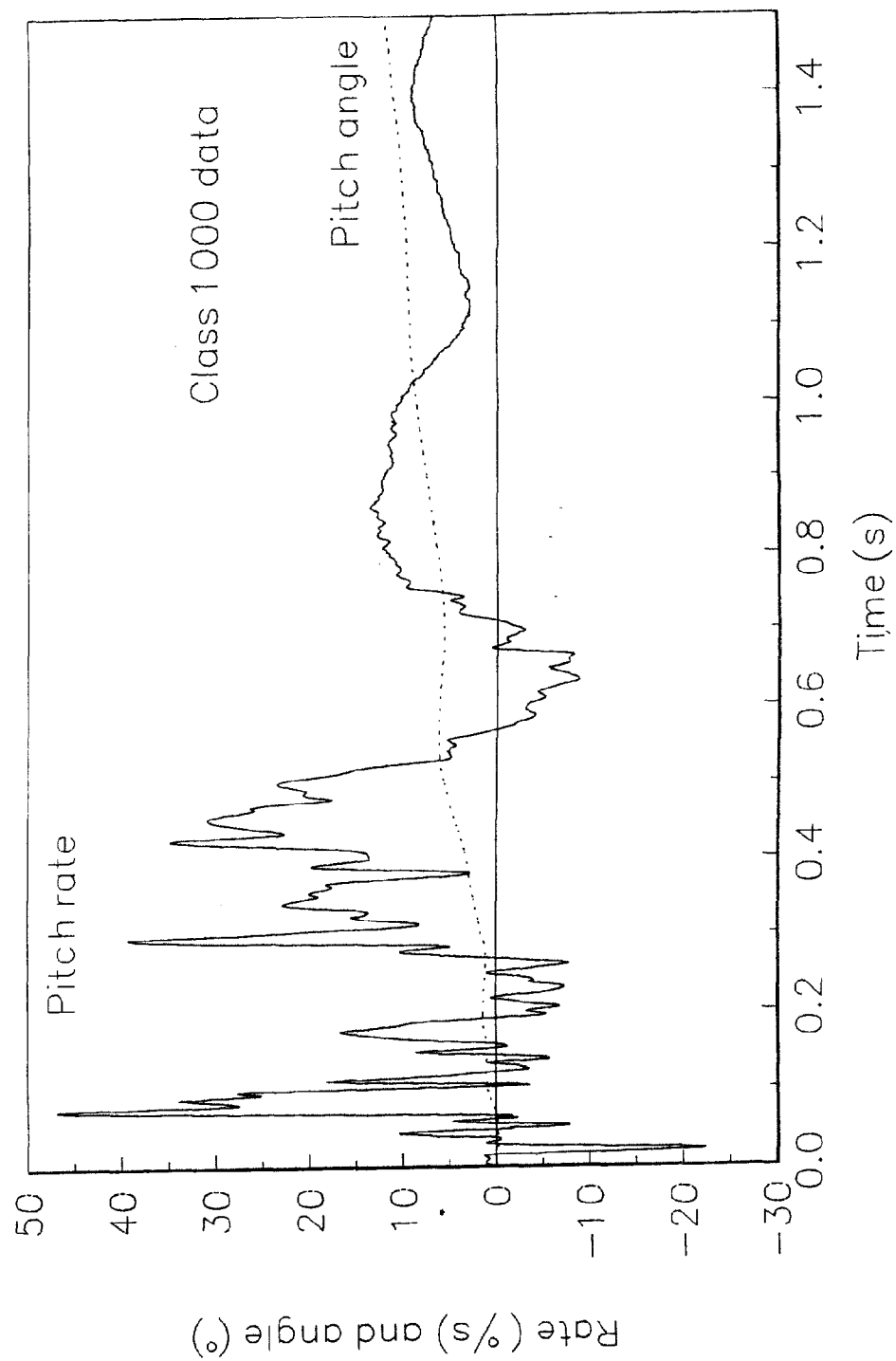


Figure 17. Pitch rate and angle vs. time, test 97S003.

Test No. 97S003
Roll rate and angle vs. time

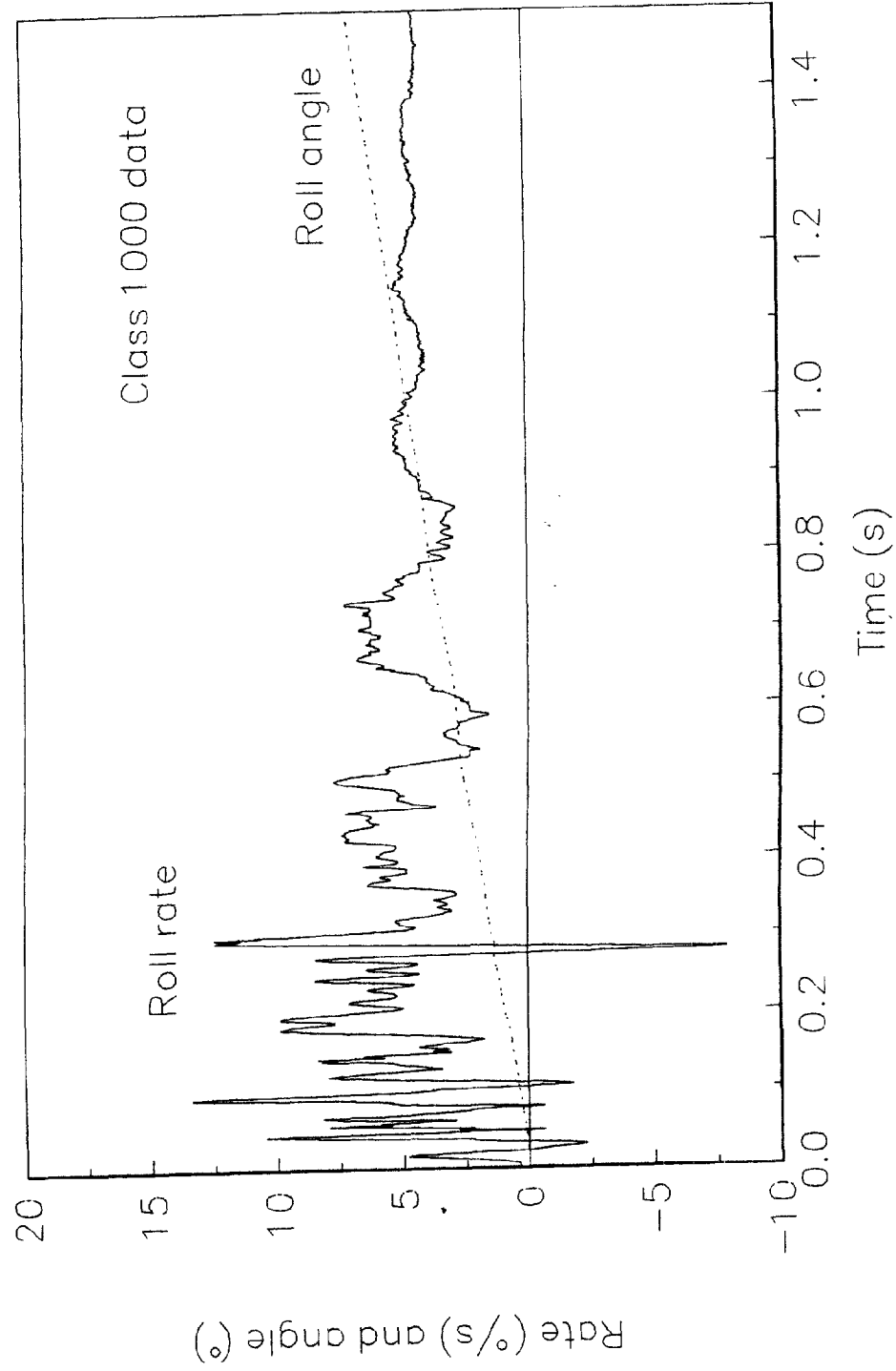


Figure 18. Roll rate and angle vs. time, test 97S003.

Test No. 97S003
Yaw rate and angle vs. time

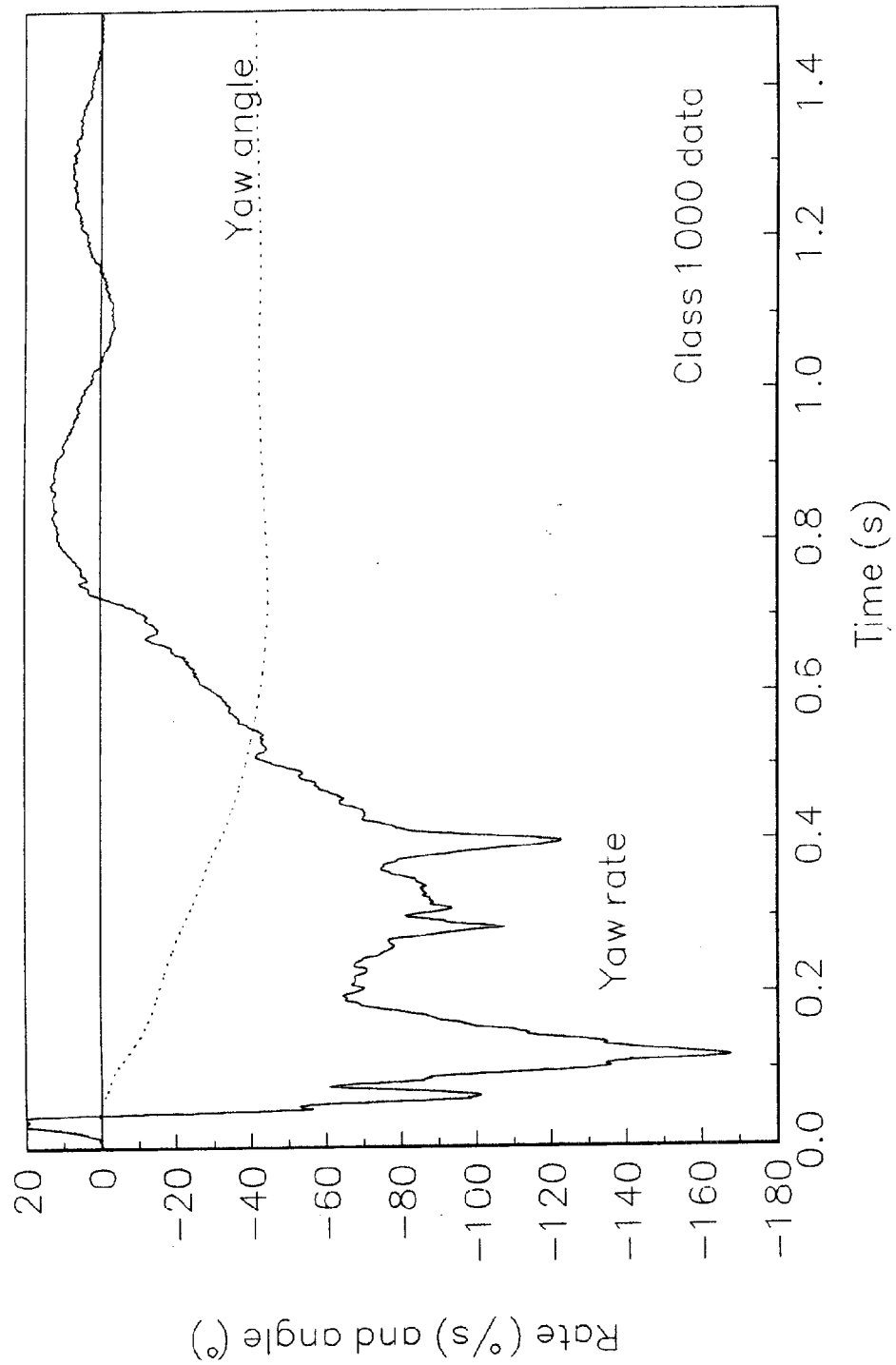


Figure 19. Yaw rate and angle vs. time, test 97S003.

APPENDIX B. DATA PLOTS FROM INSTRUMENTED SID/HIII.

Test No. 97S003
X-axis, head acceleration vs. time

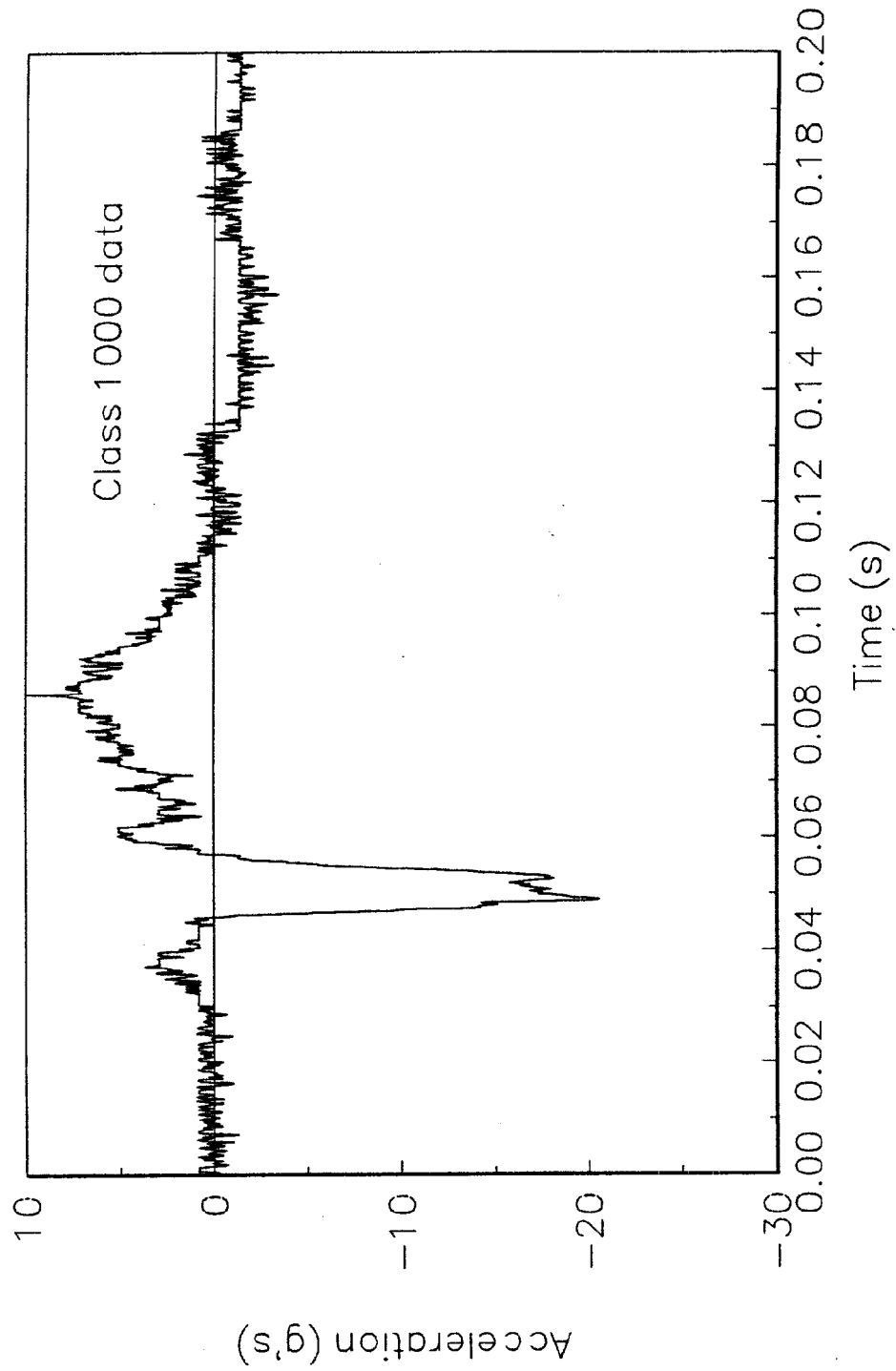


Figure 20. Acceleration vs. time, X-axis head, test 97S003.

Test No. 97S003
Y-axis, head acceleration vs. time

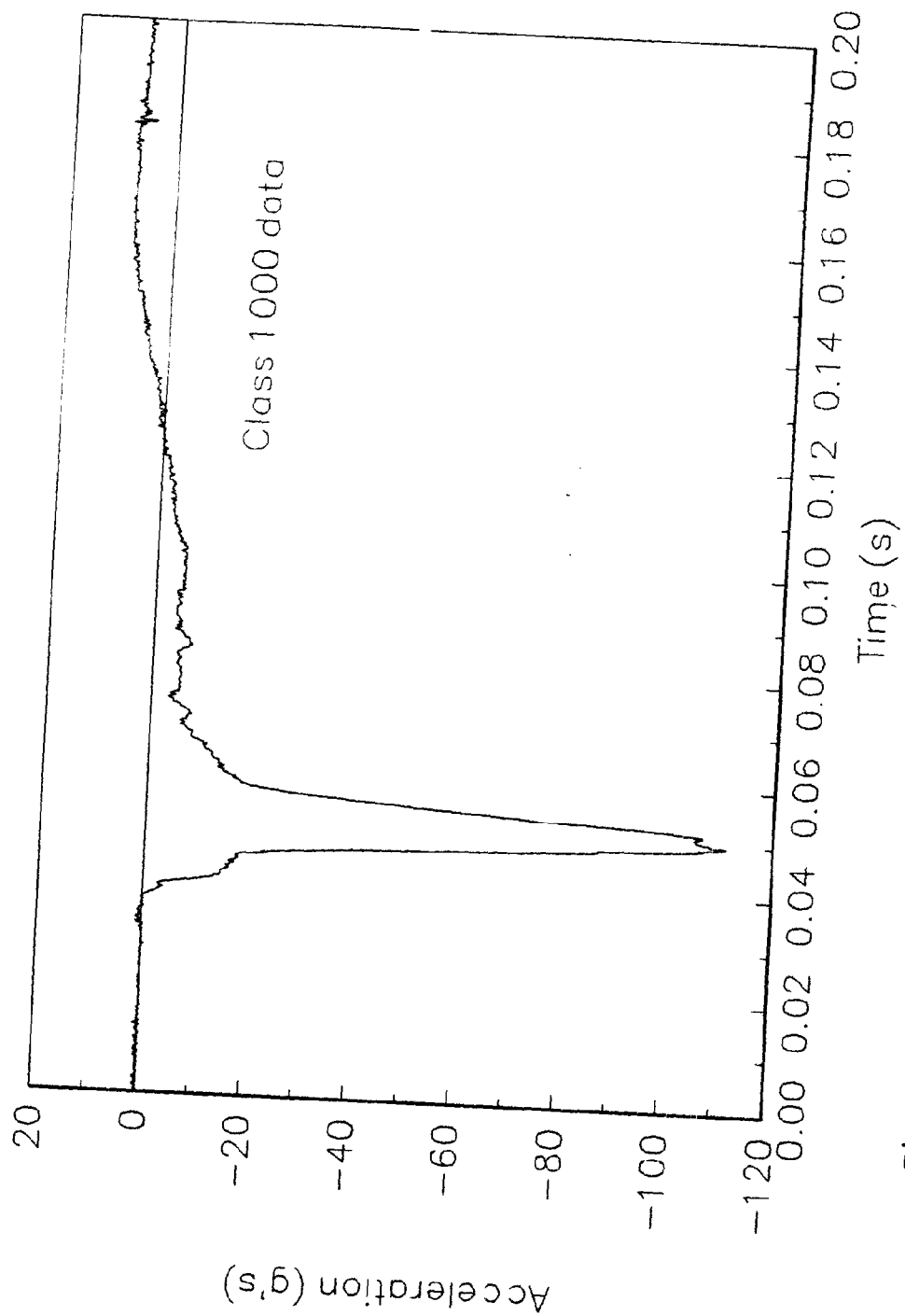


Figure 21. Acceleration vs. time, Y-axis head, test 97S003.

Test No. 97S003
Z-axis, head acceleration vs. time

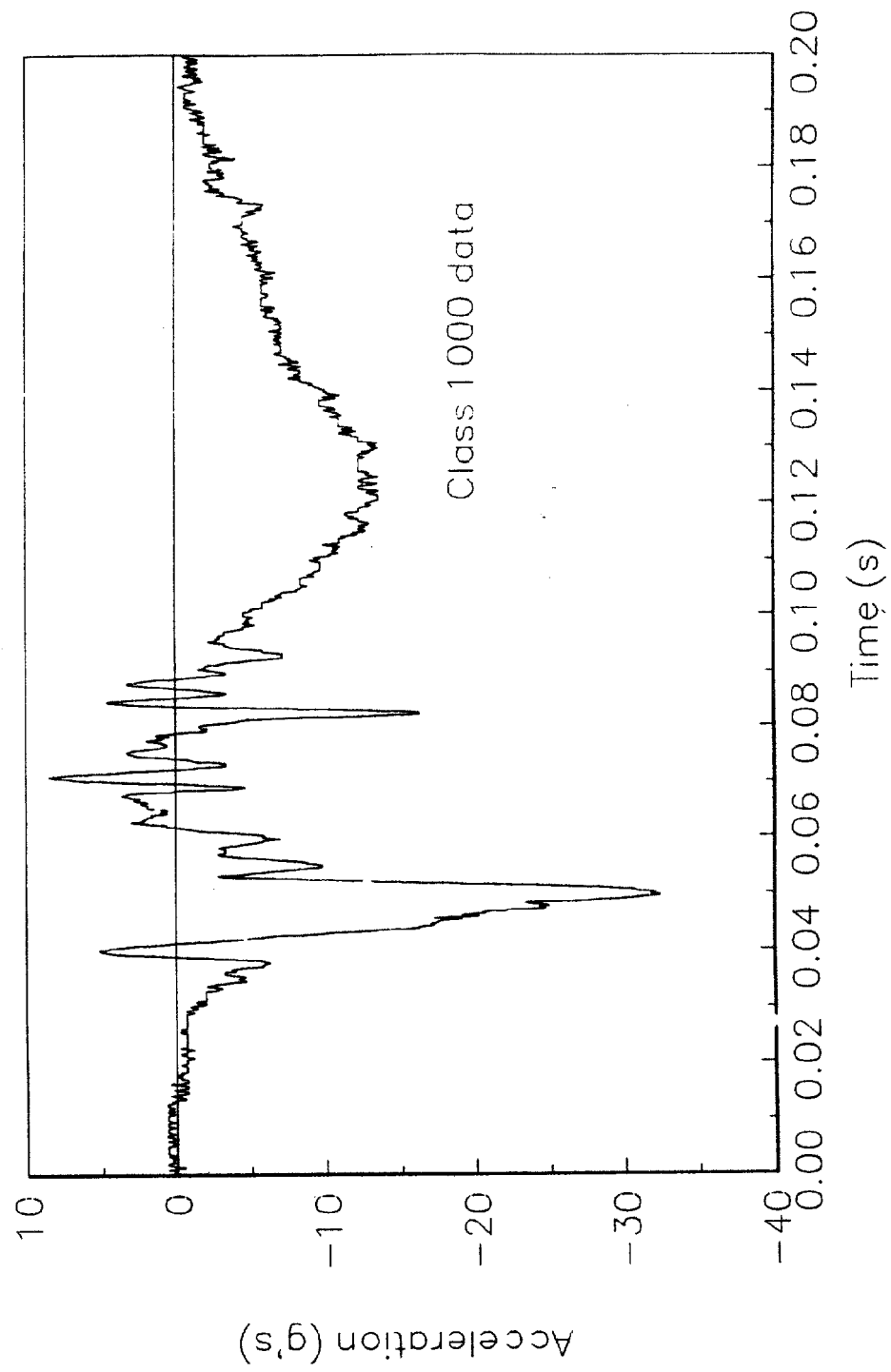


Figure 22. Acceleration vs. time, Z-axis head, test 97S003.

Test No. 97S003
X-axis neck force vs. time

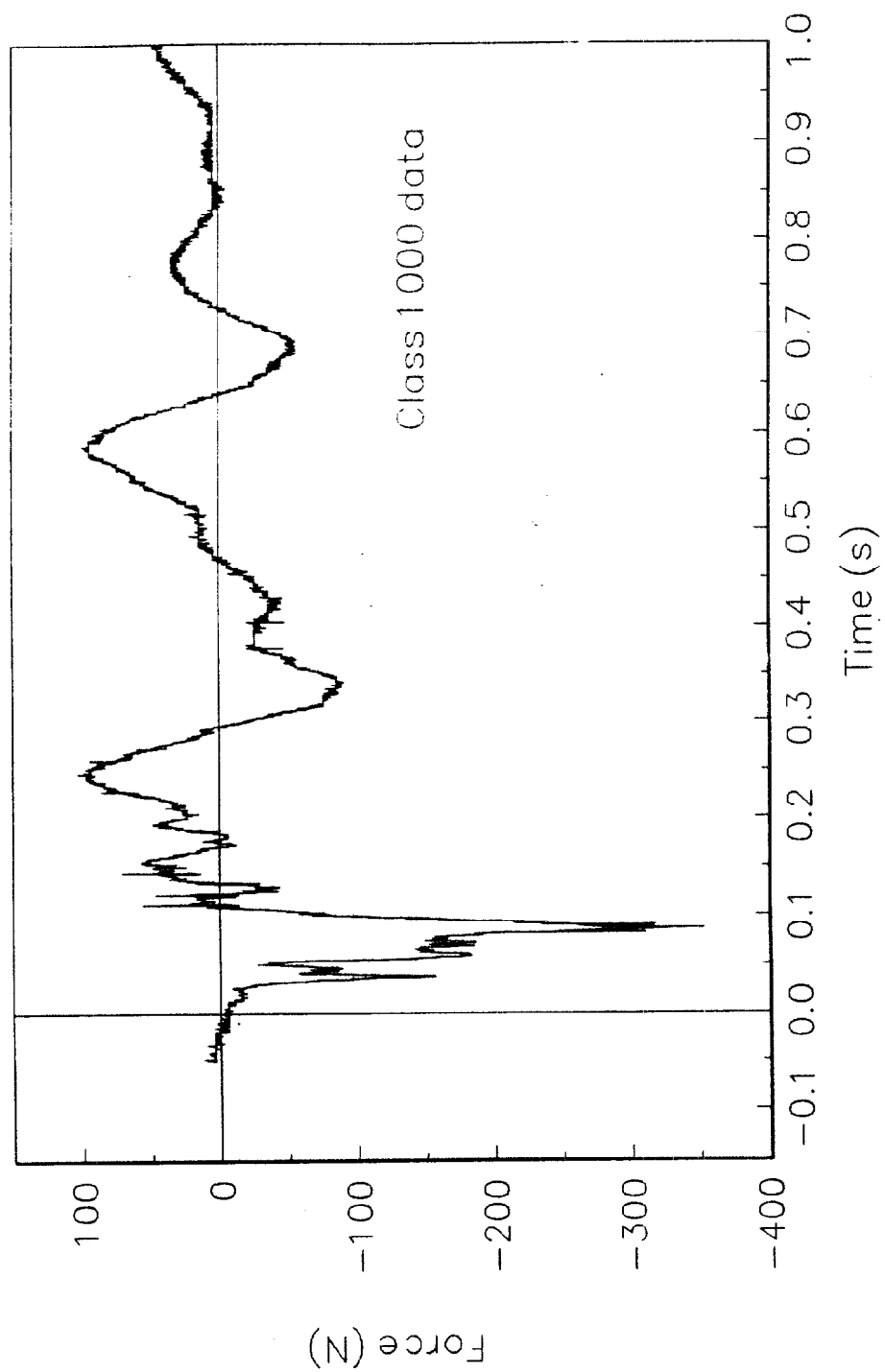


Figure 23. Force vs. time, X-axis neck, test 97S003.

Test No. 97S003
Y-axis neck force vs. time

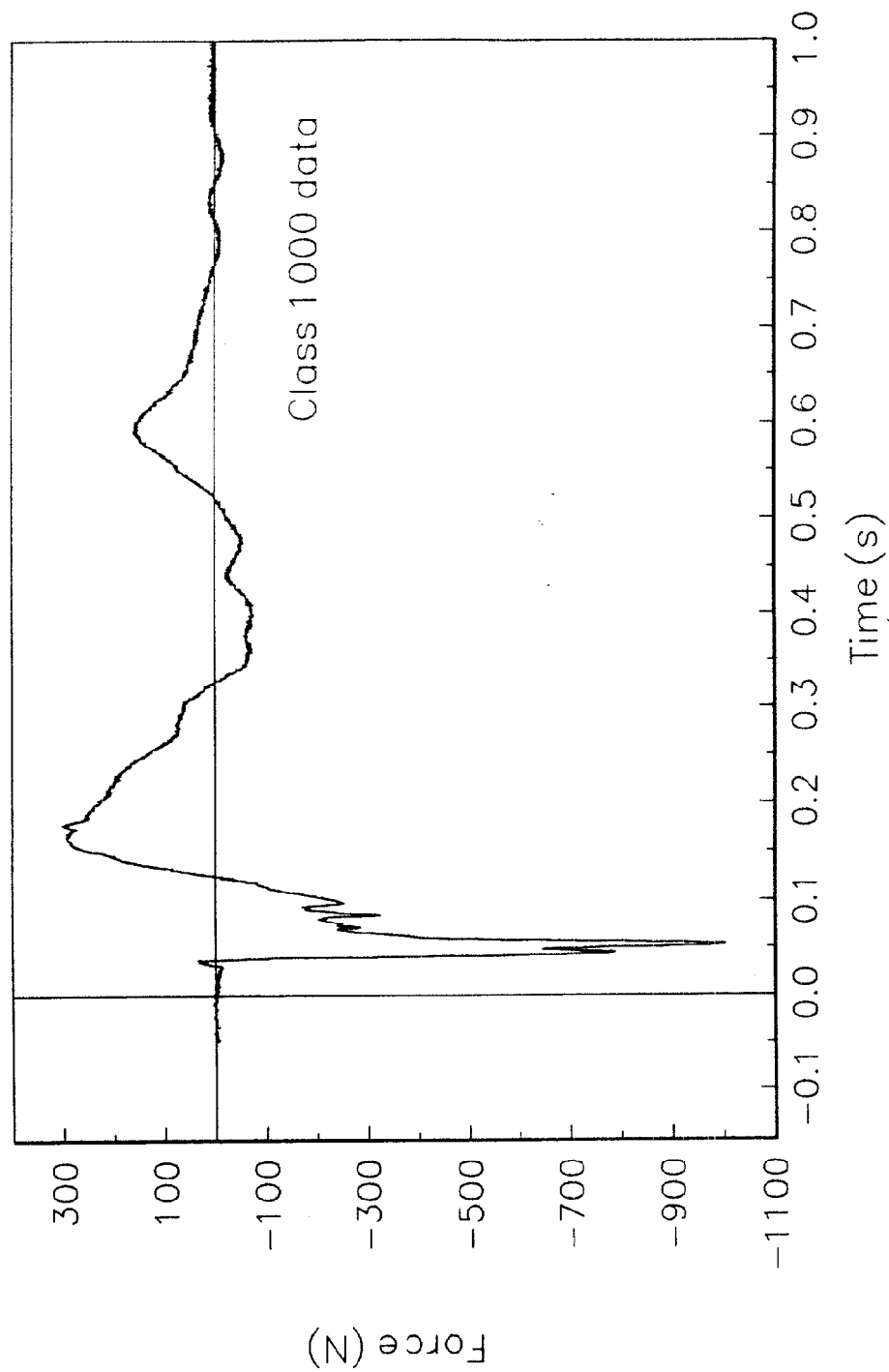


Figure 24. Force vs. time, Y-axis neck, test 97S003.

Test No. 97S003
Z-axis neck force vs. time

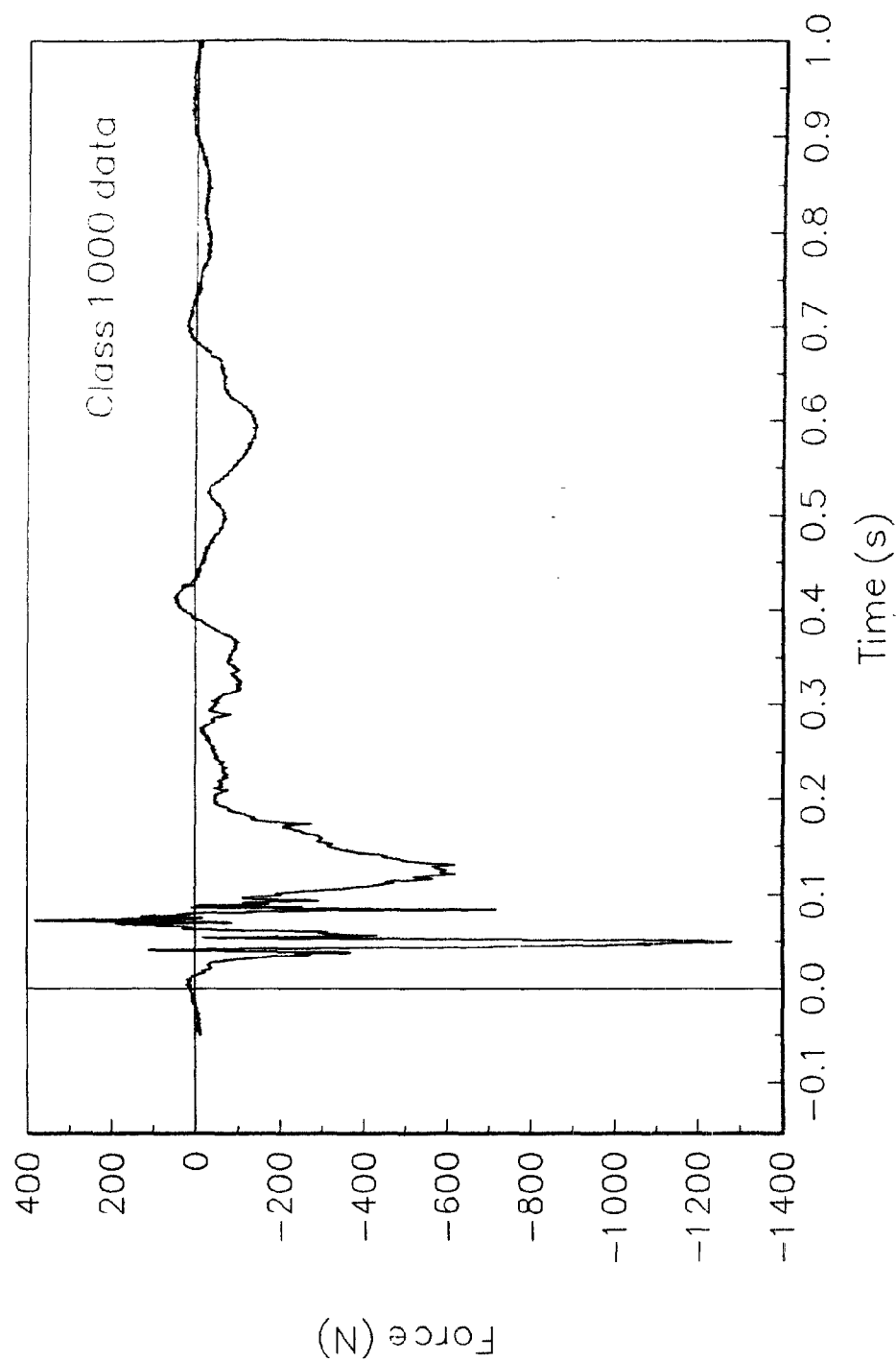


Figure 25. Force vs. time, Z-axis, neck, test 97S003.

Test No. 97S003
X-axis neck moment vs. time

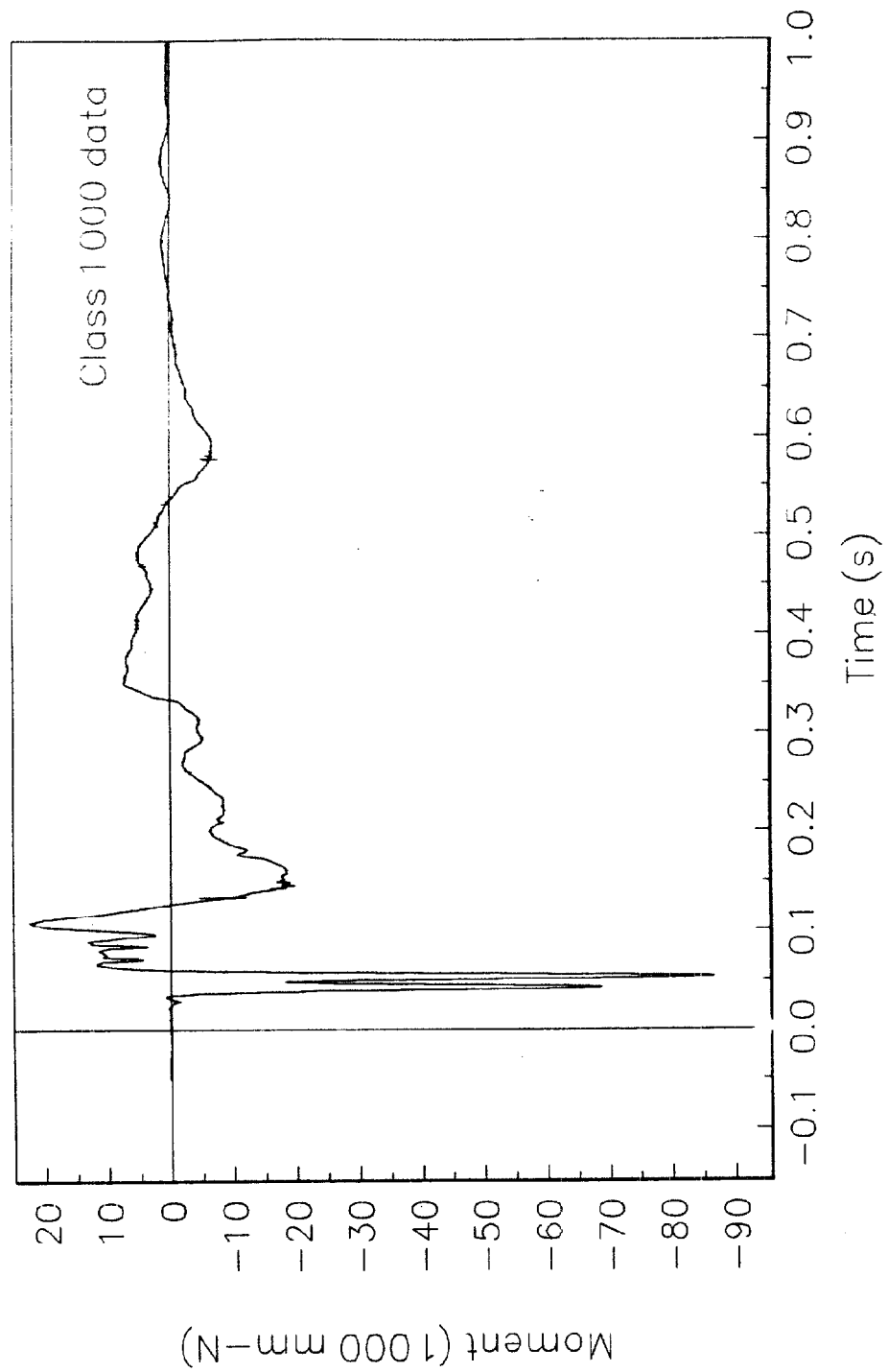


Figure 26. Moment vs. time, X-axis neck, test 97S003.

Test No. 97S003
Y-axis neck moment vs. time

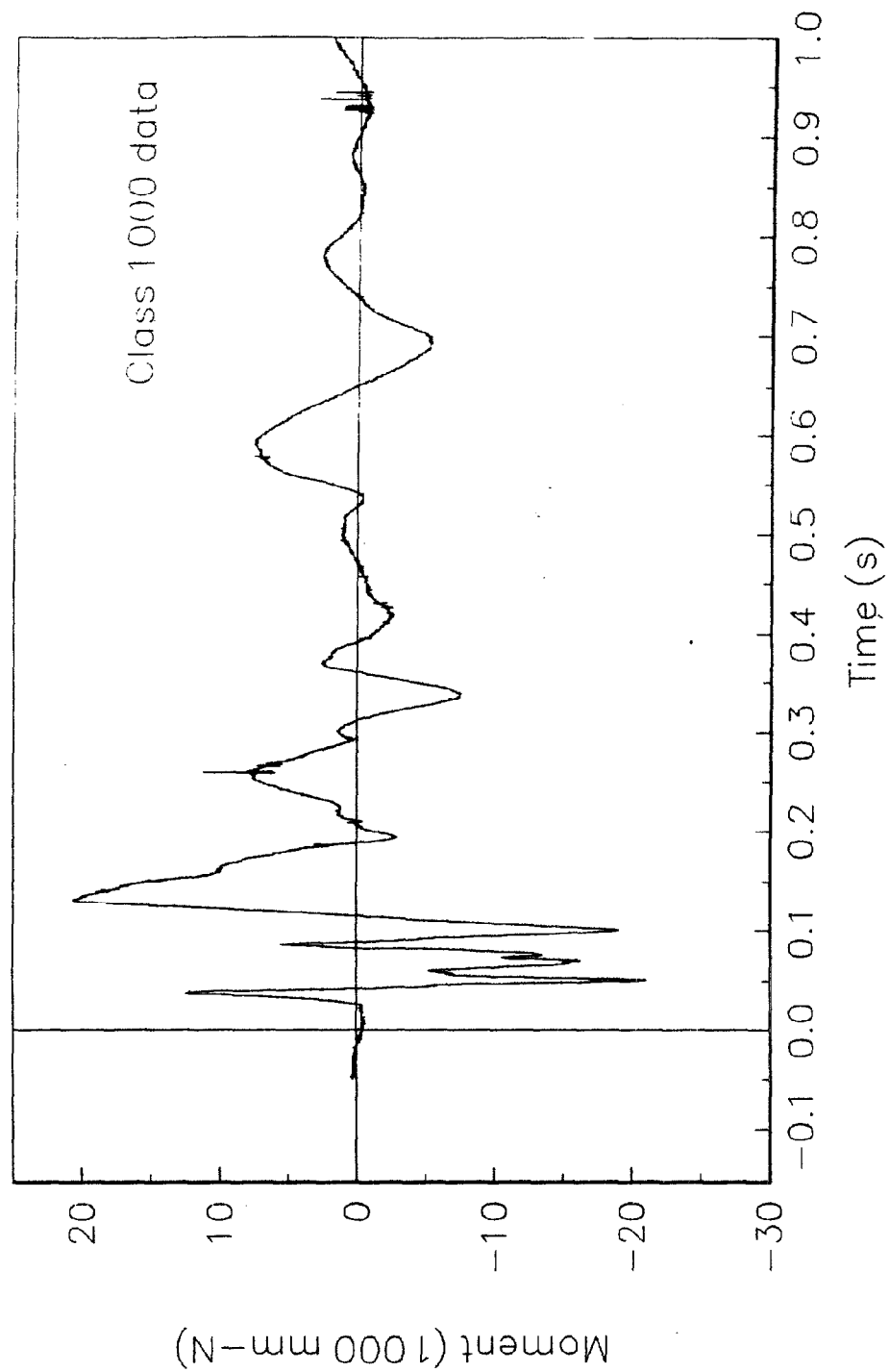


Figure 27. Moment vs. time, Y-axis neck, test 97S003.

Test No. 97S003
Z-axis neck moment vs. time

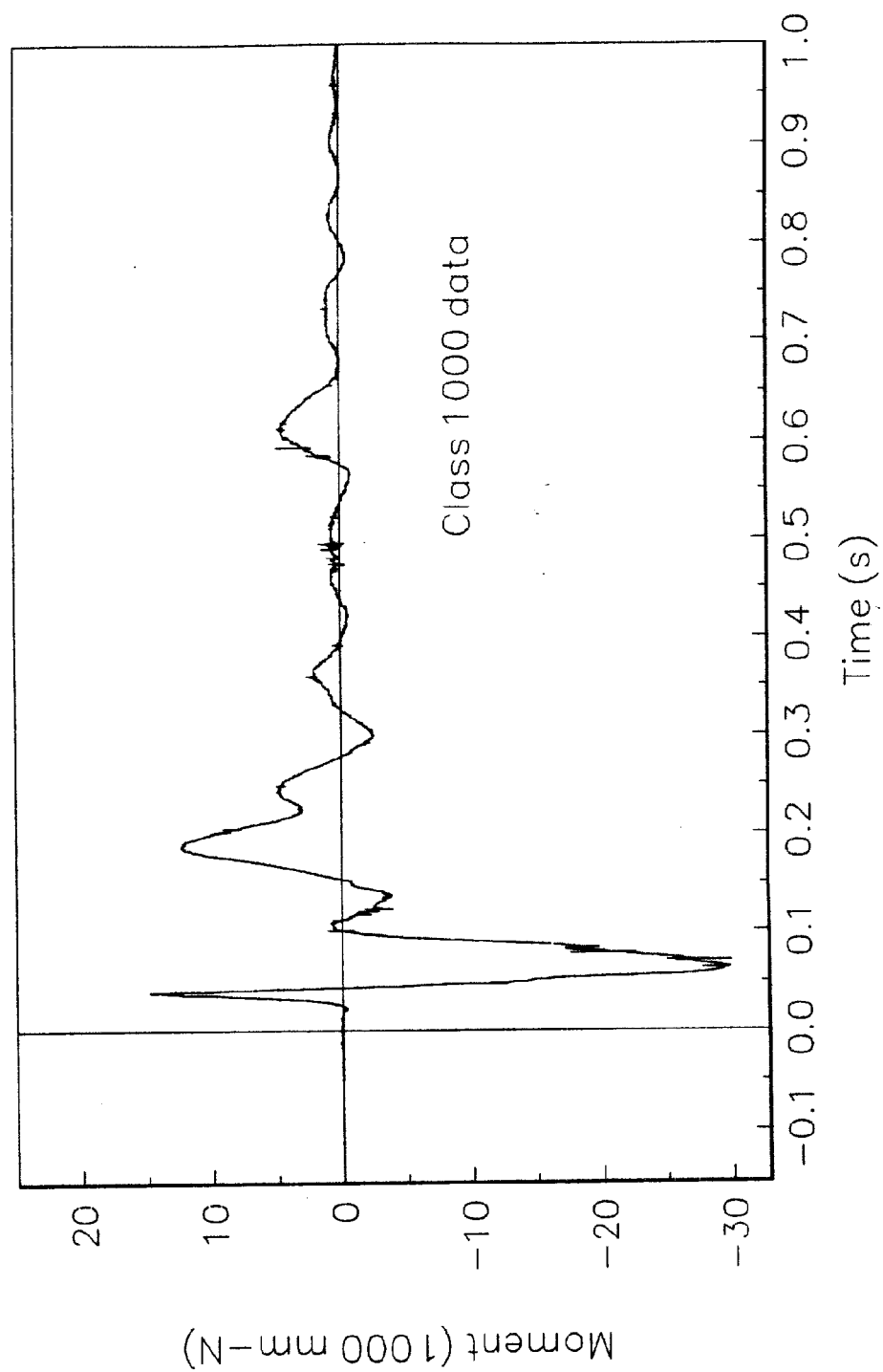


Figure 28. Moment vs. time, Z-axis neck, test 97S003.

Test No. 97S003

Primary upper rib acceleration

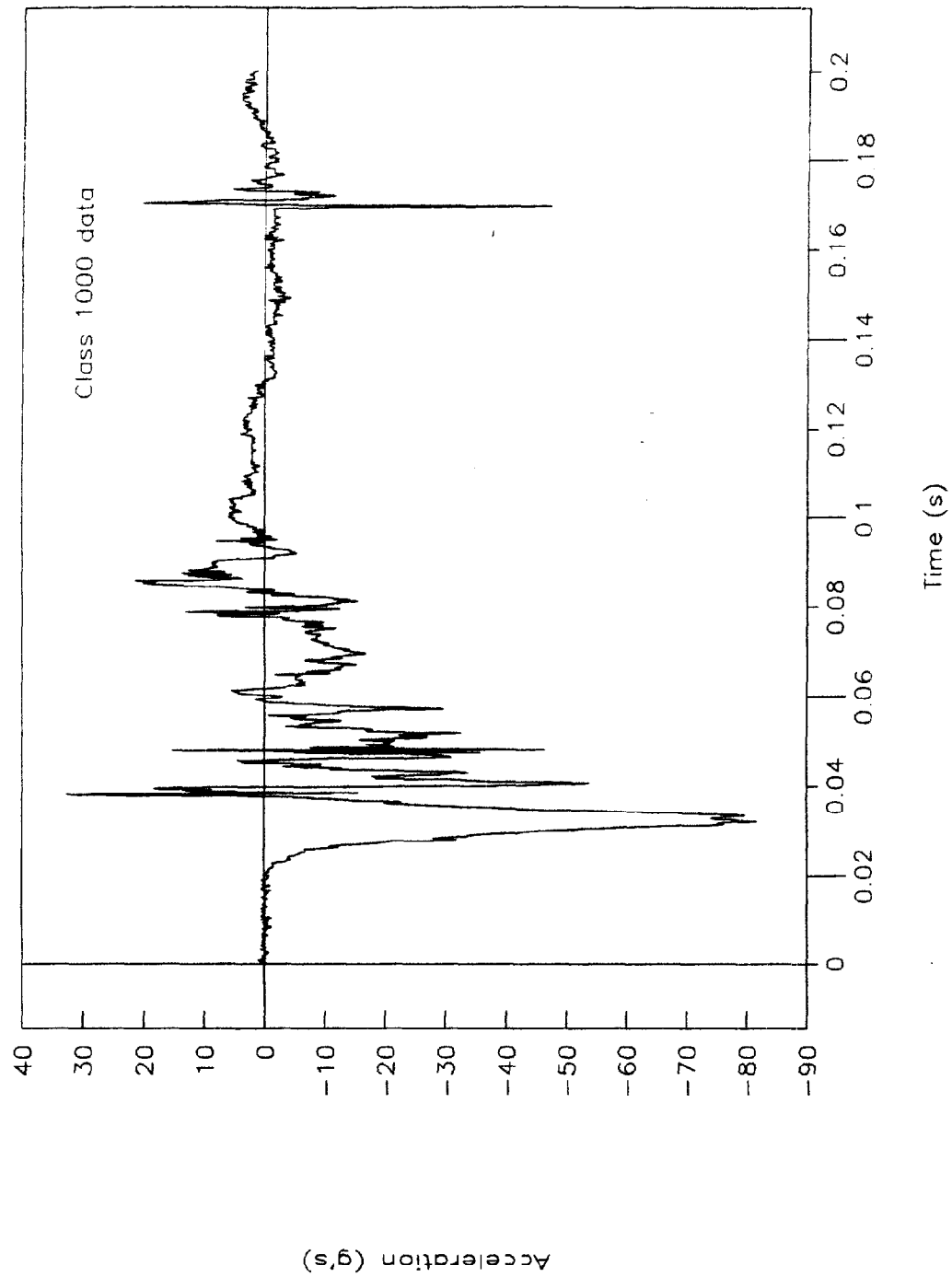


Figure 29. Acceleration vs. time, primary upper rib, test 97S003.

Test No. 97S003
Redundant upper rib acceleration

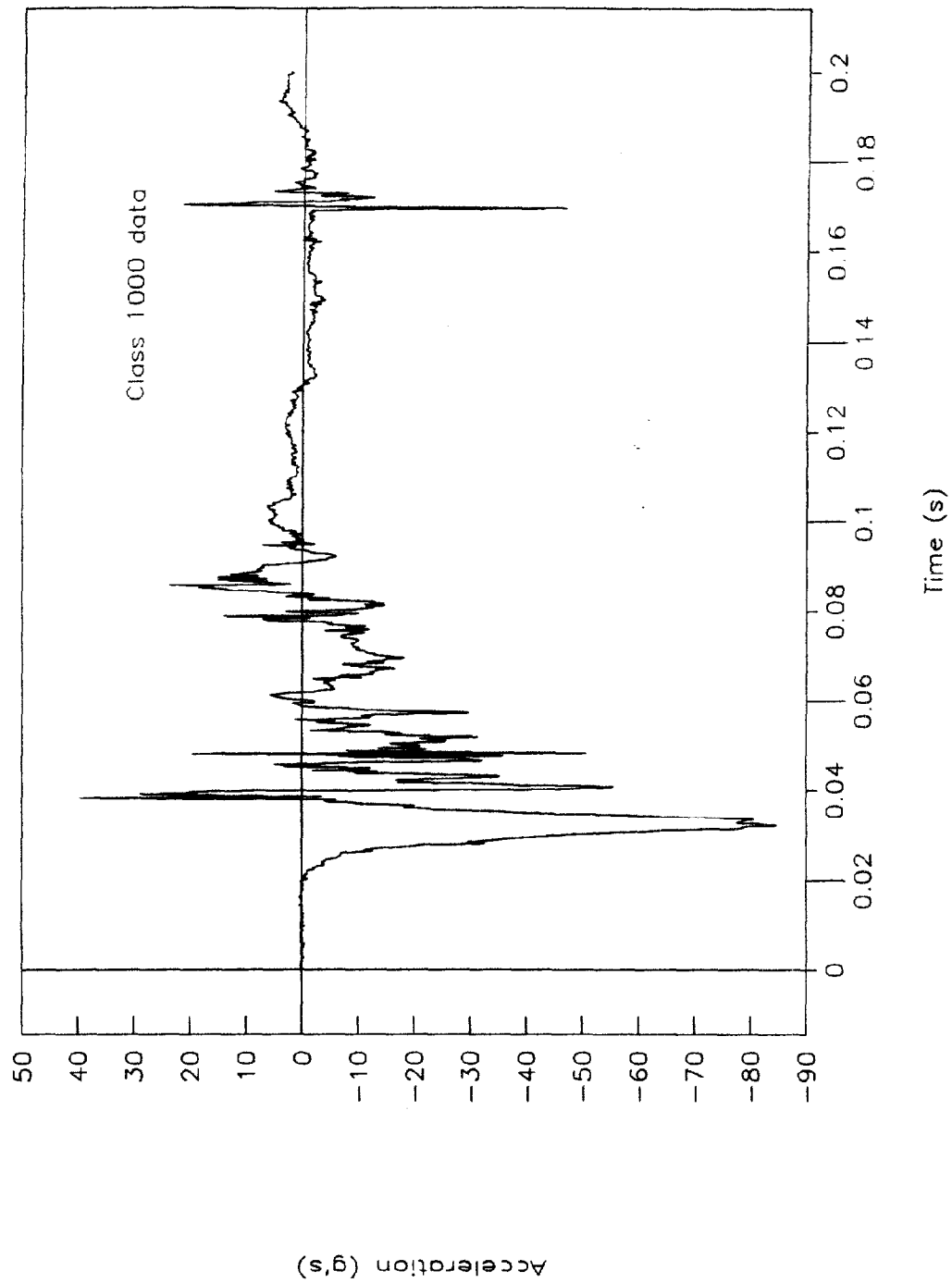


Figure 30. Acceleration vs. time, redundant upper rib, test 97S003.

Test No. 97S003

Primary lower rib acceleration

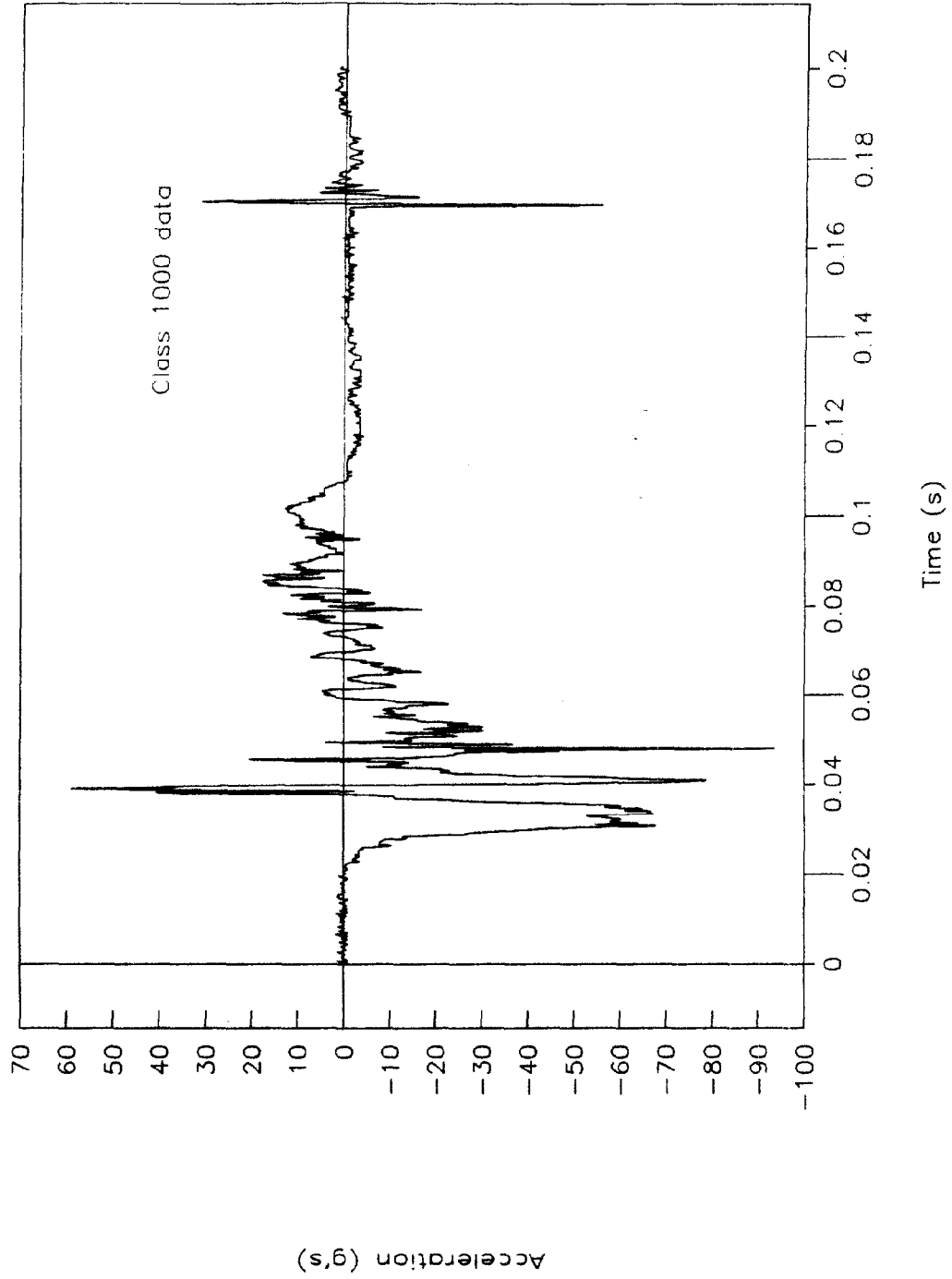


Figure 31. Acceleration vs. time, primary lower rib, test 97S003.

Test No. 97S003

Redundant lower rib acceleration

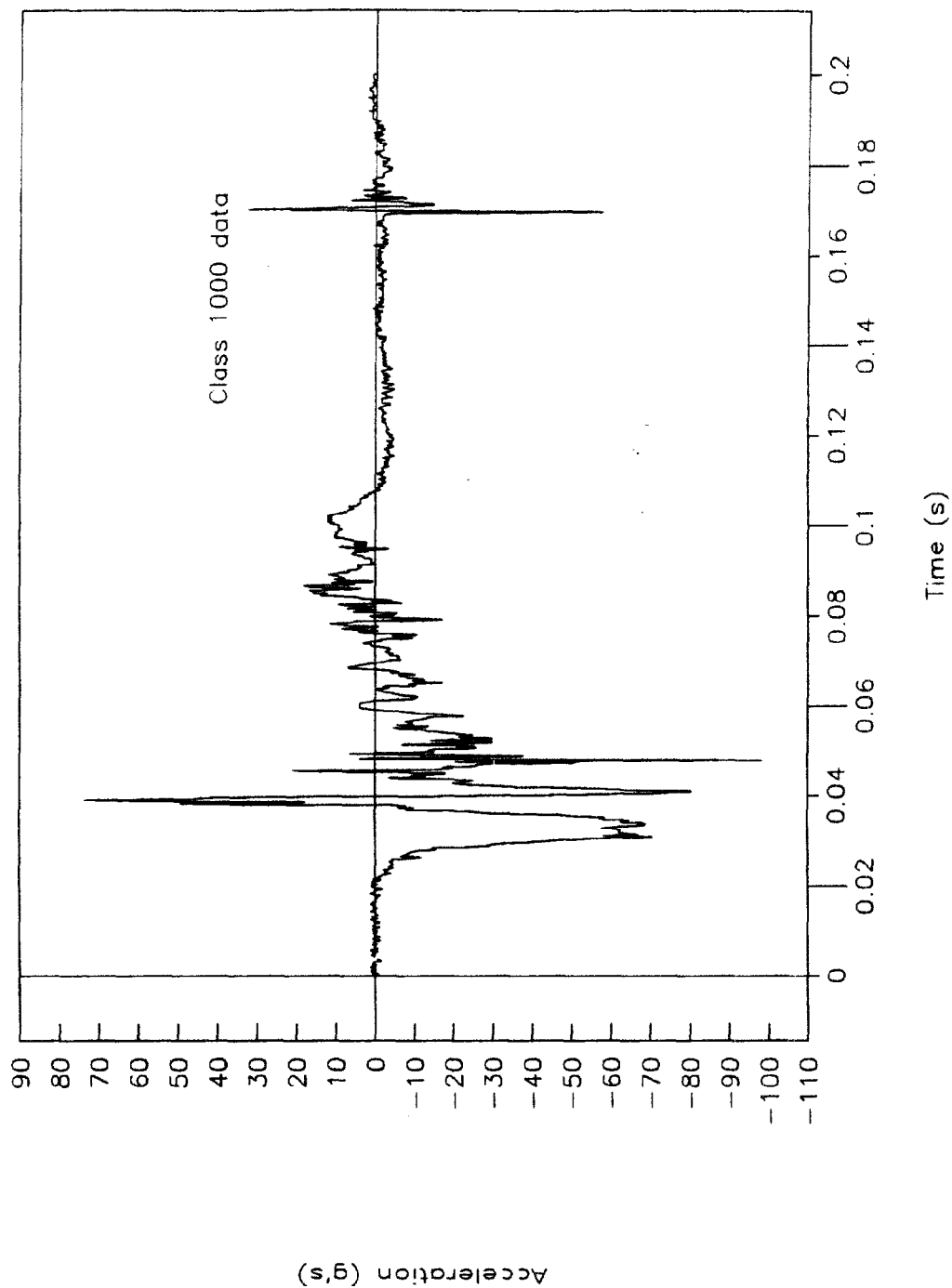


Figure 32. Acceleration vs. time, redundant lower rib, test 97S003.

Test No. 97S003

Primary T12 spine acceleration

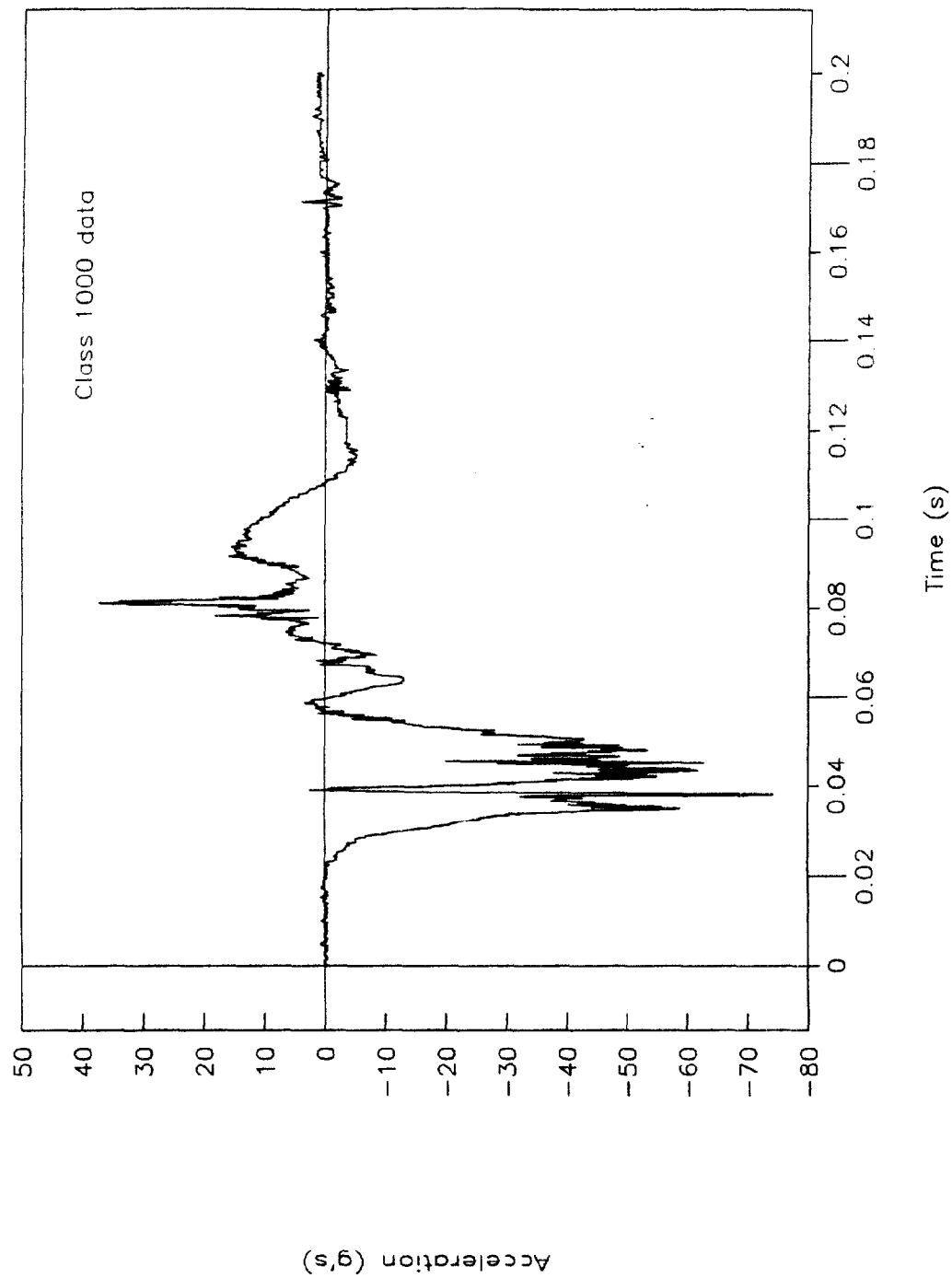


Figure 33. Acceleration vs. time, primary T12 spine, test 97S003.

Test No. 97S003

Redundant T12 spine acceleration

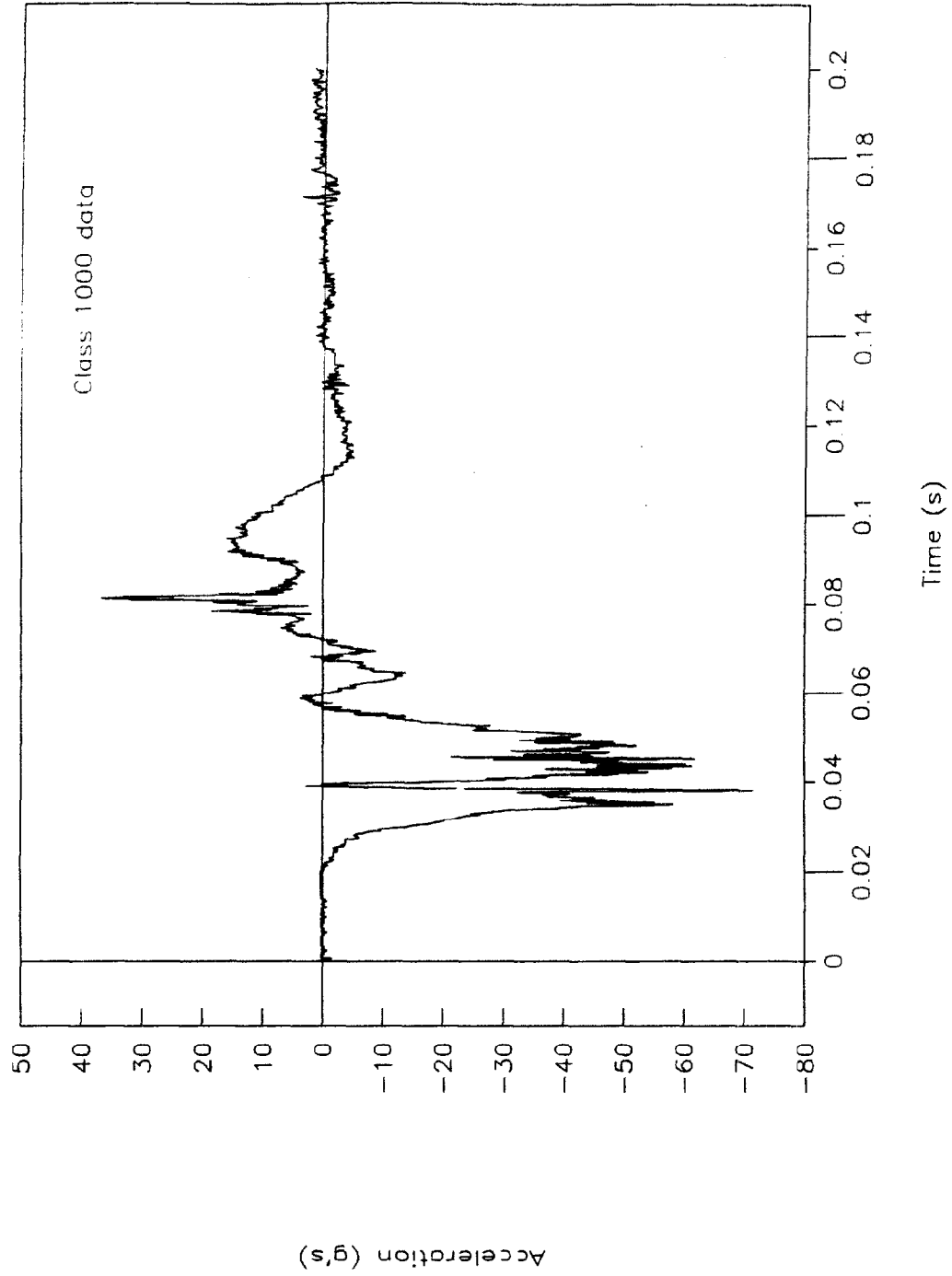


Figure 34. Acceleration vs. time, redundant T12 spine, test 97S003.

Test No. 97S003

Y-axis pelvis acceleration

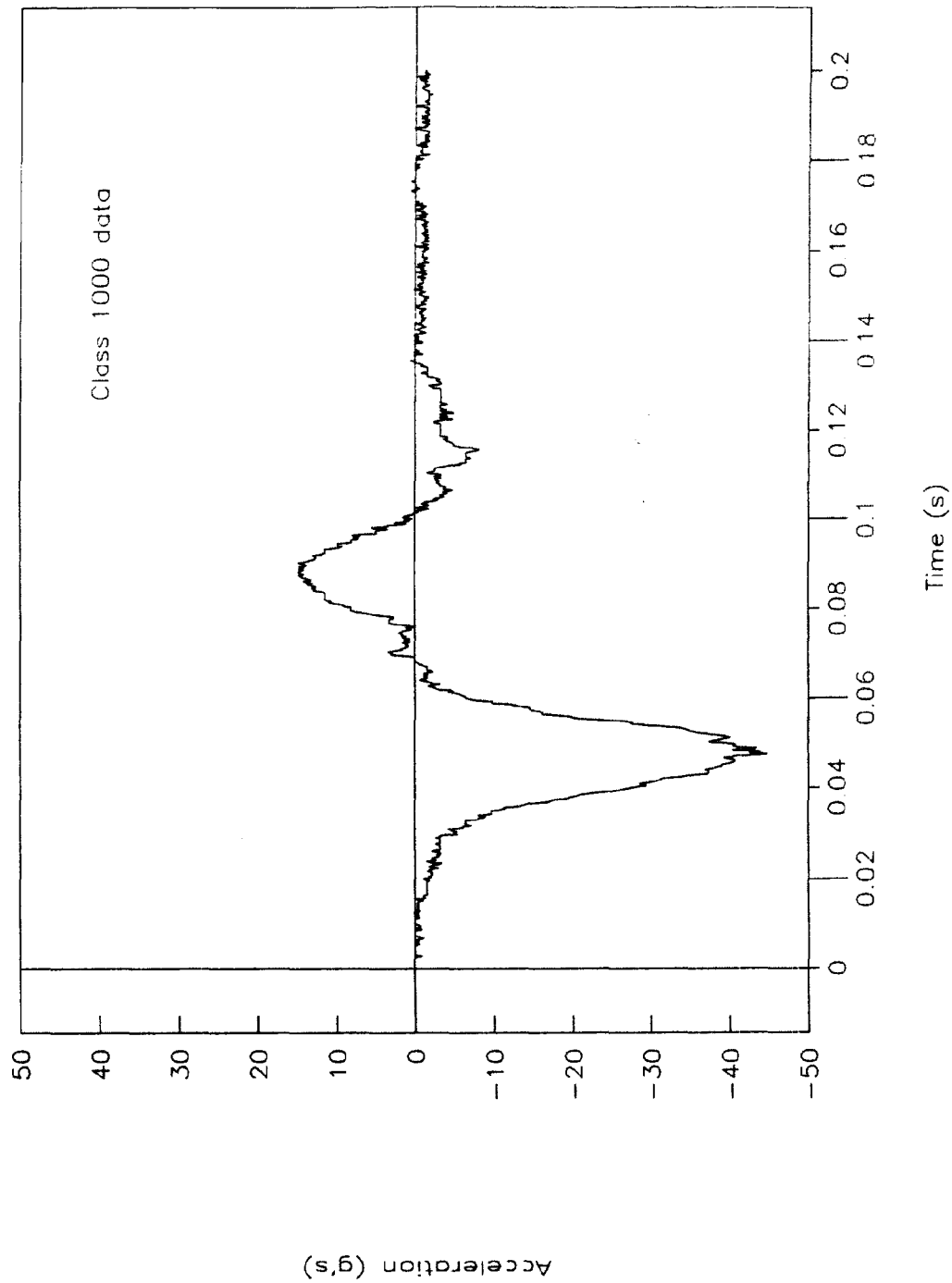
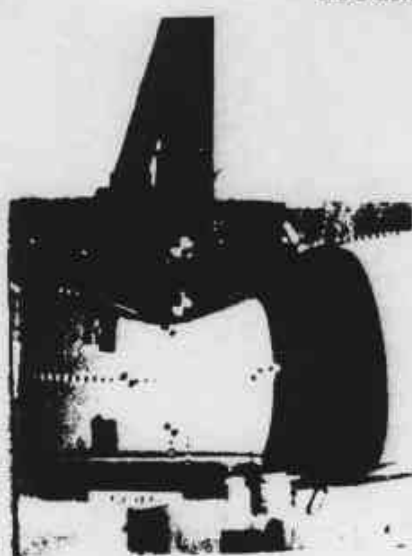
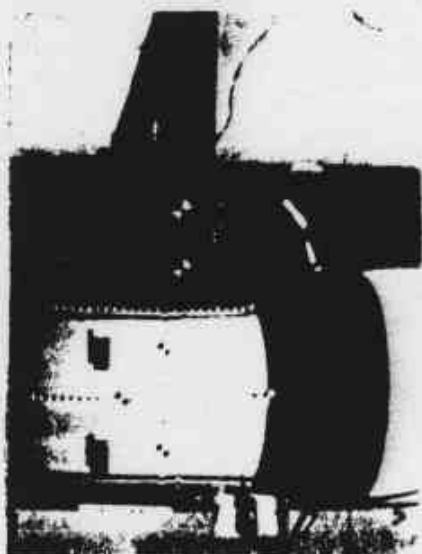


Figure 35. Acceleration vs. time, Y-axis pelvis, test 97S003.

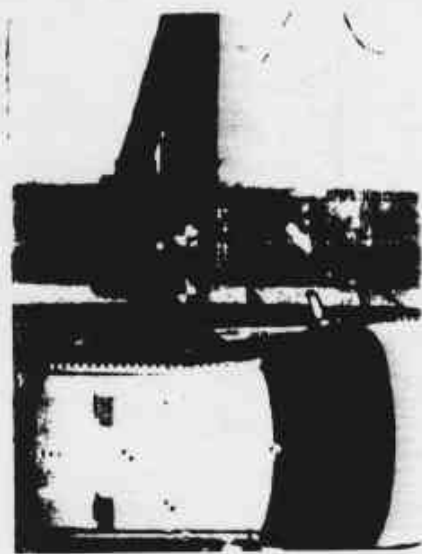
APPENDIX C. TEST PHOTOGRAPHS.



0.000 s



0.026 s



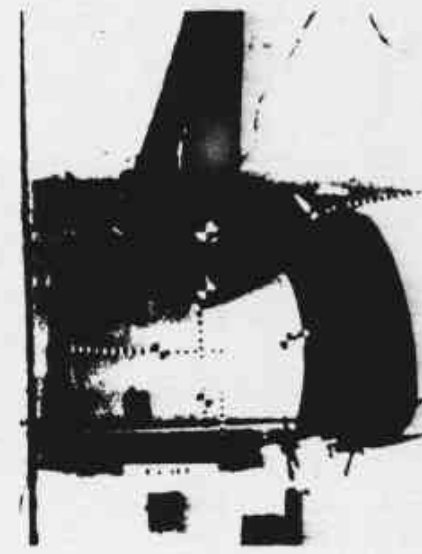
0.100 s



0.848 s



0.306 s

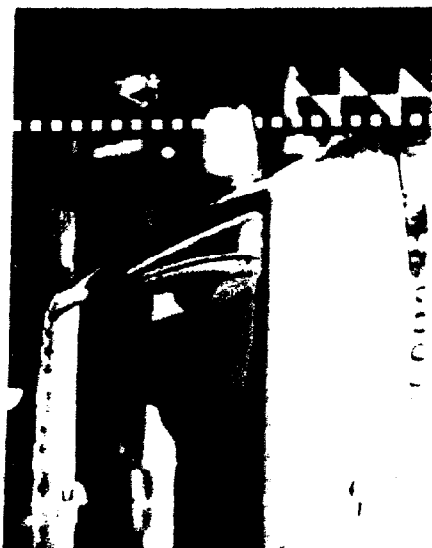


0.146 s

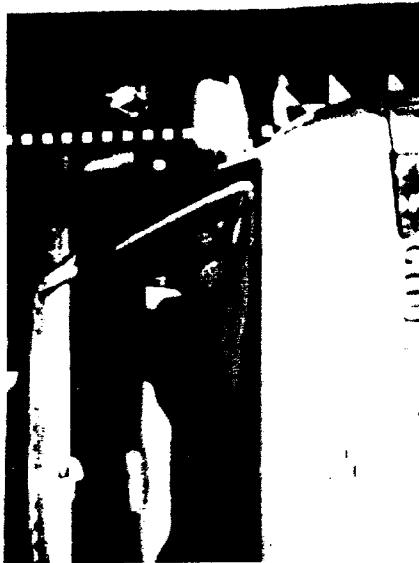
Figure 36. Test photographs during impact, test 9/5001.



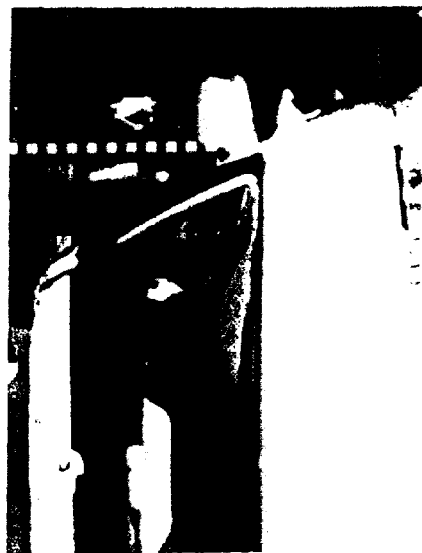
0.000 s



0.018 s



0.032 s



0.038 s



0.052 s



0.066 s

Figure 16. Test photographs during impact, test 978003 (continued).

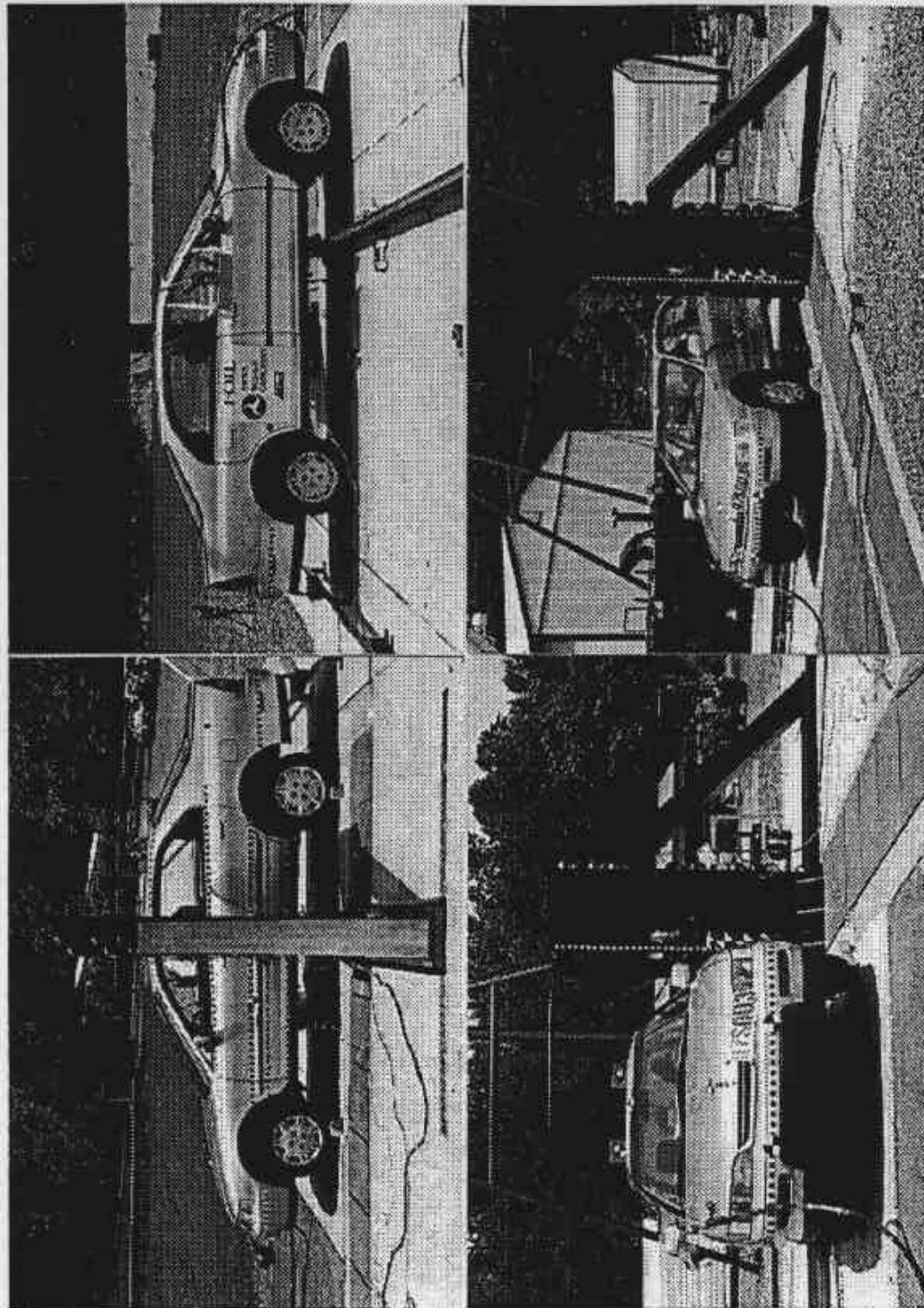


Figure 37. Pretest photographs, test 97S0003.

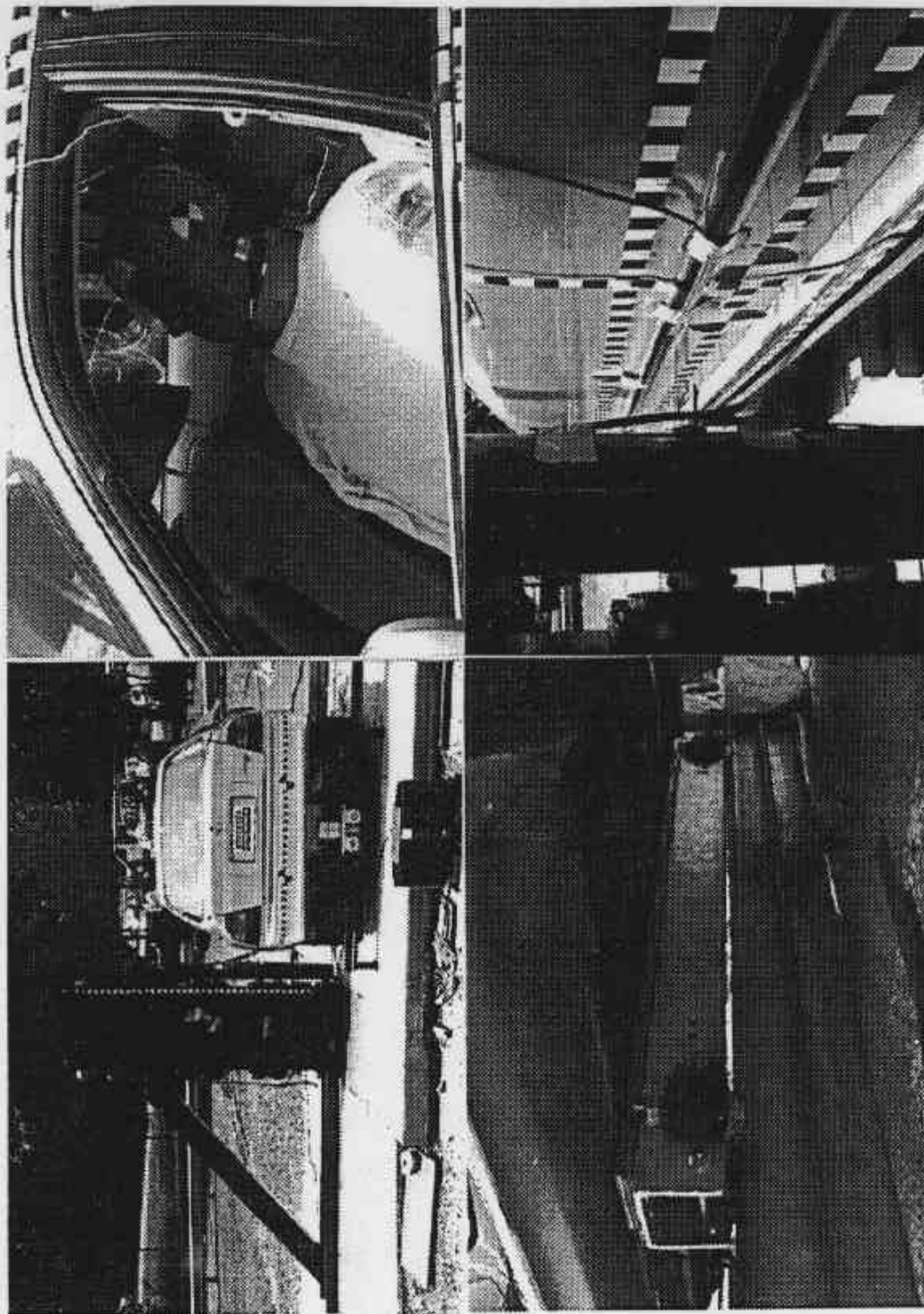


Figure 37. Pretest photographs, test 97S003 (continued).

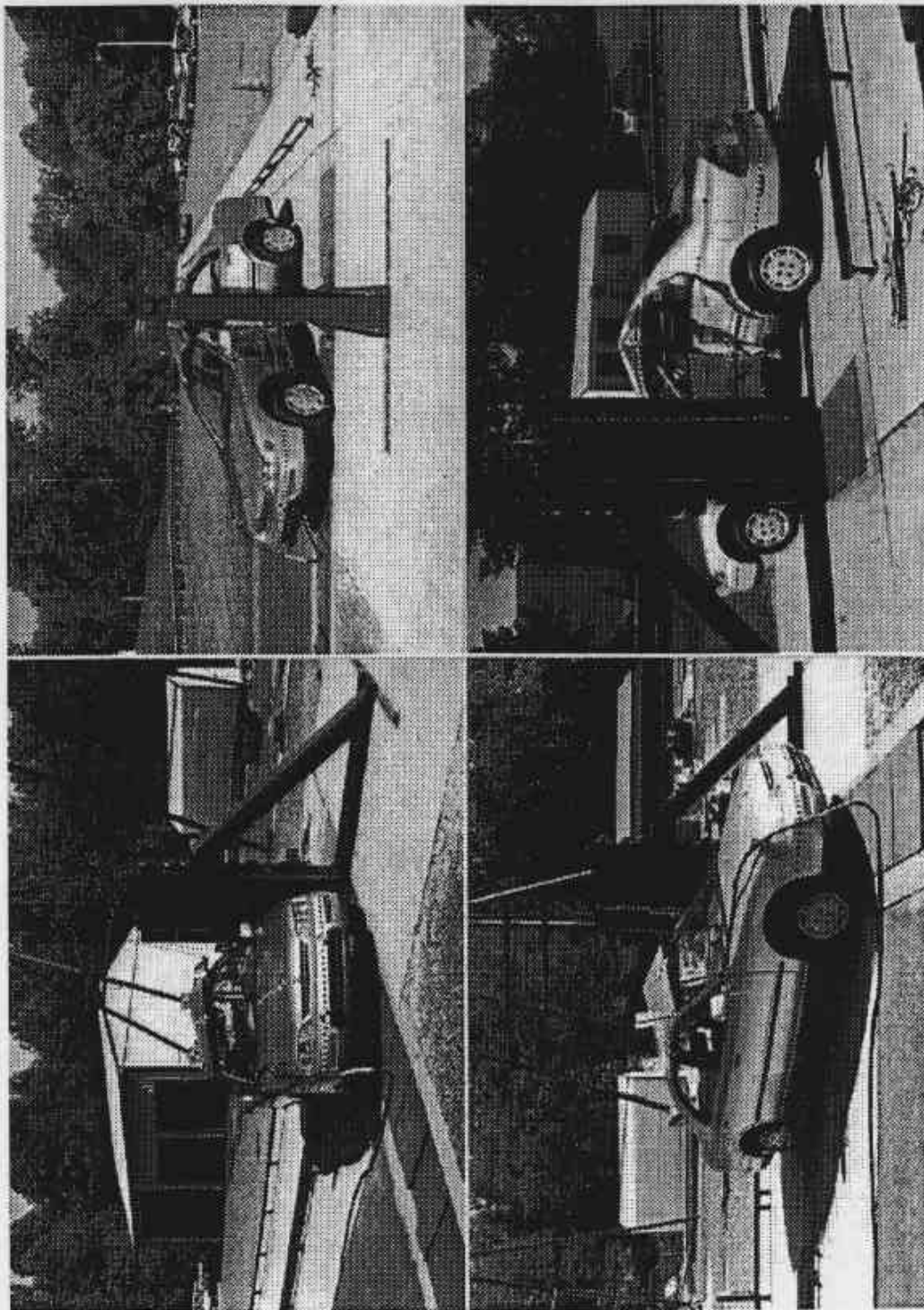


Figure 38. Post-test photographs, test 97S003.

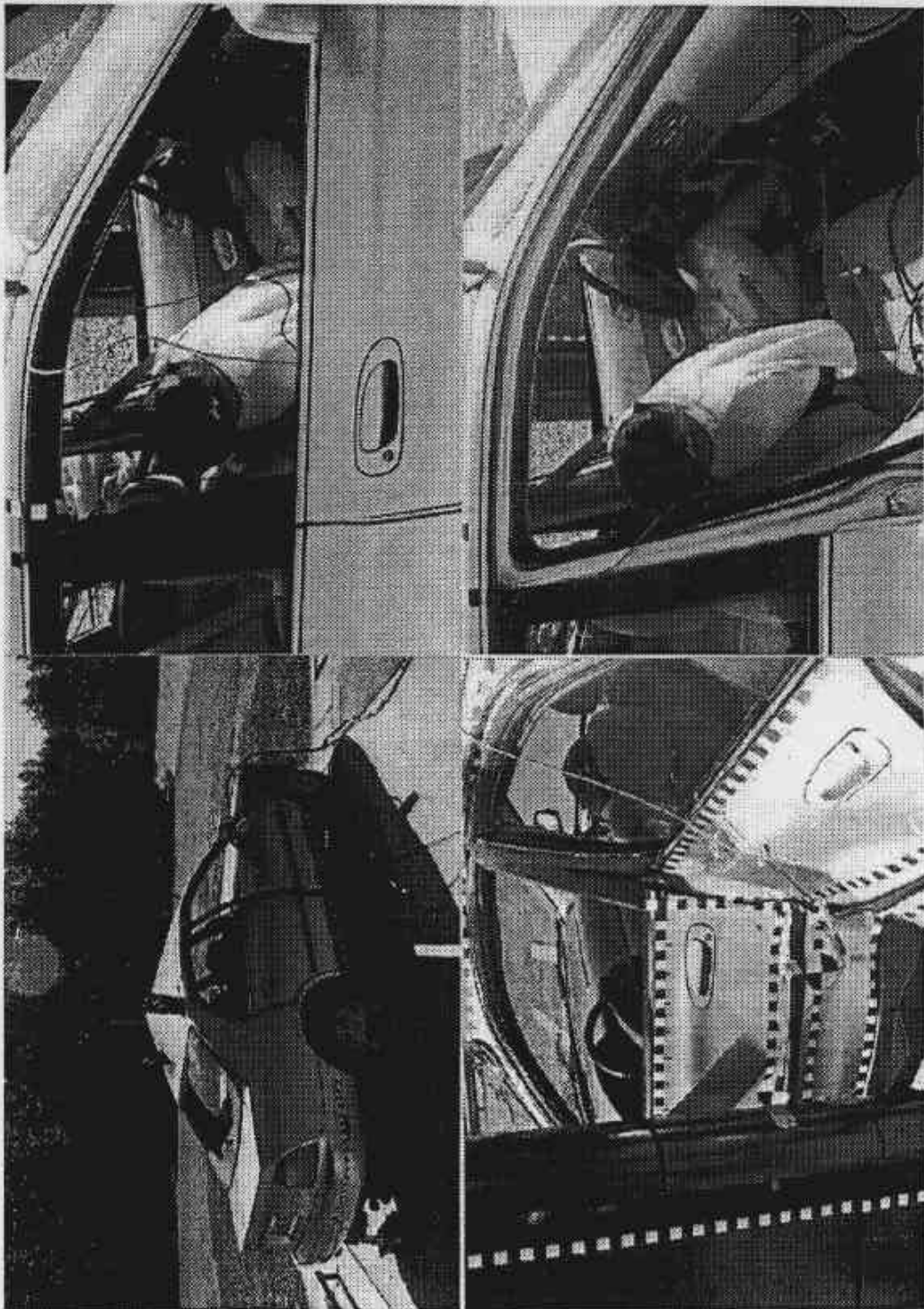


Figure 38. Post-test photographs, test 97S003 (continued).

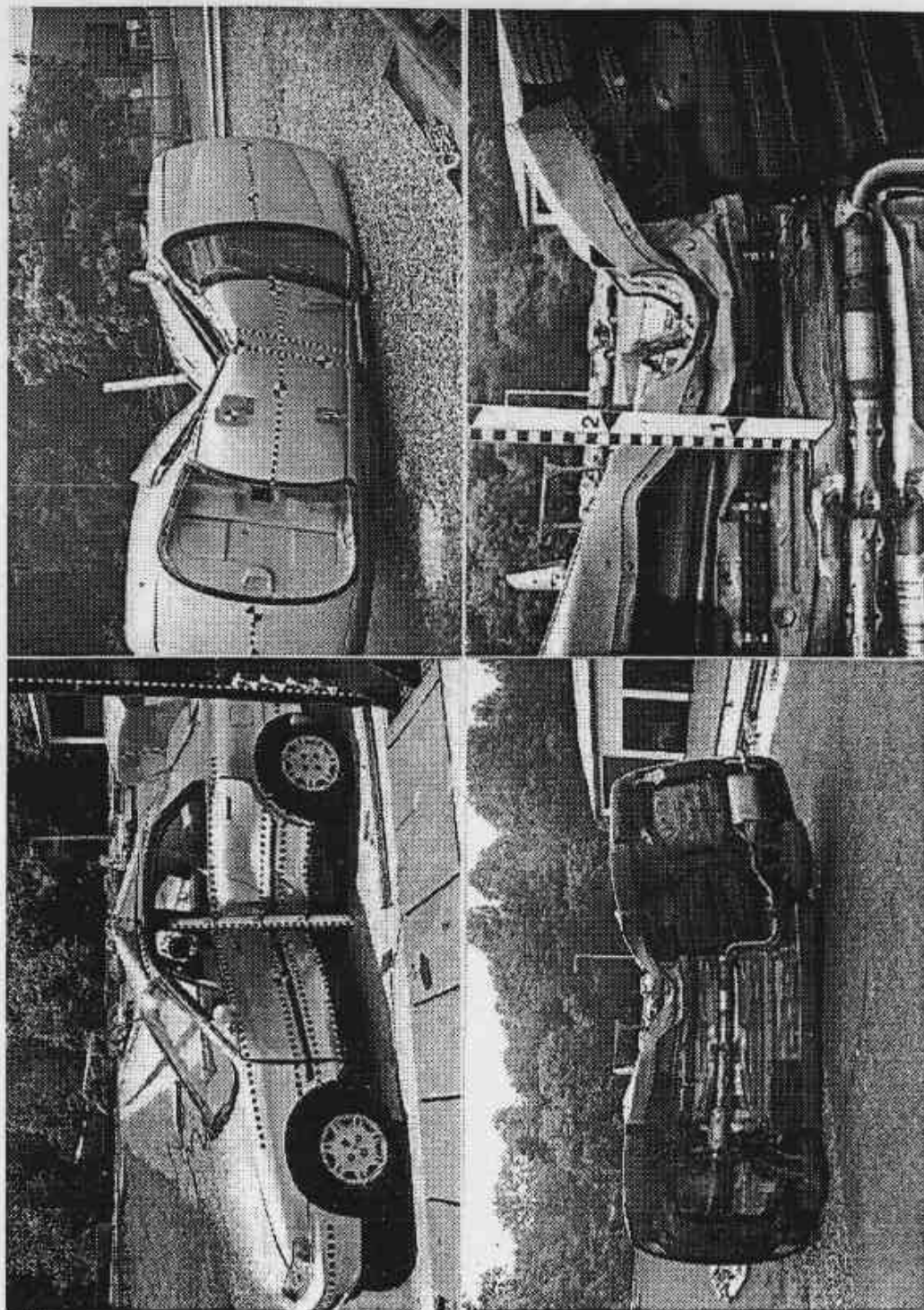


Figure 38. Post-test photographs, test 97S003 (continued).

APPENDIX D. DATA PLOTS FROM RIGID POLE LOAD CELLS.

Test No. 97S003
Bottom face lower load cell

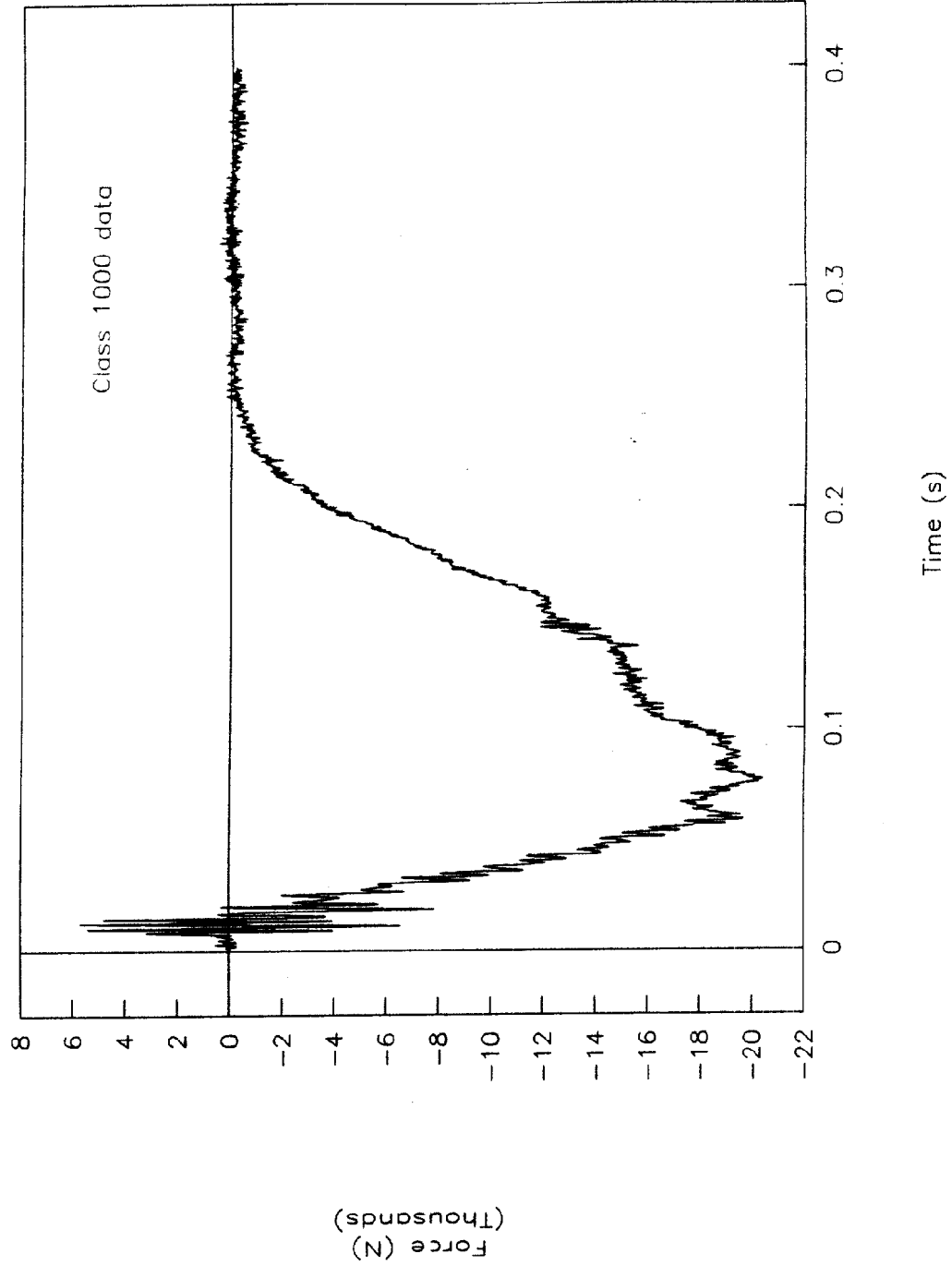


Figure 39. Rigid pole, force vs. time, bottom face lower load cell, test 97S003.

Test No. 97S003

Bottom face upper load cell

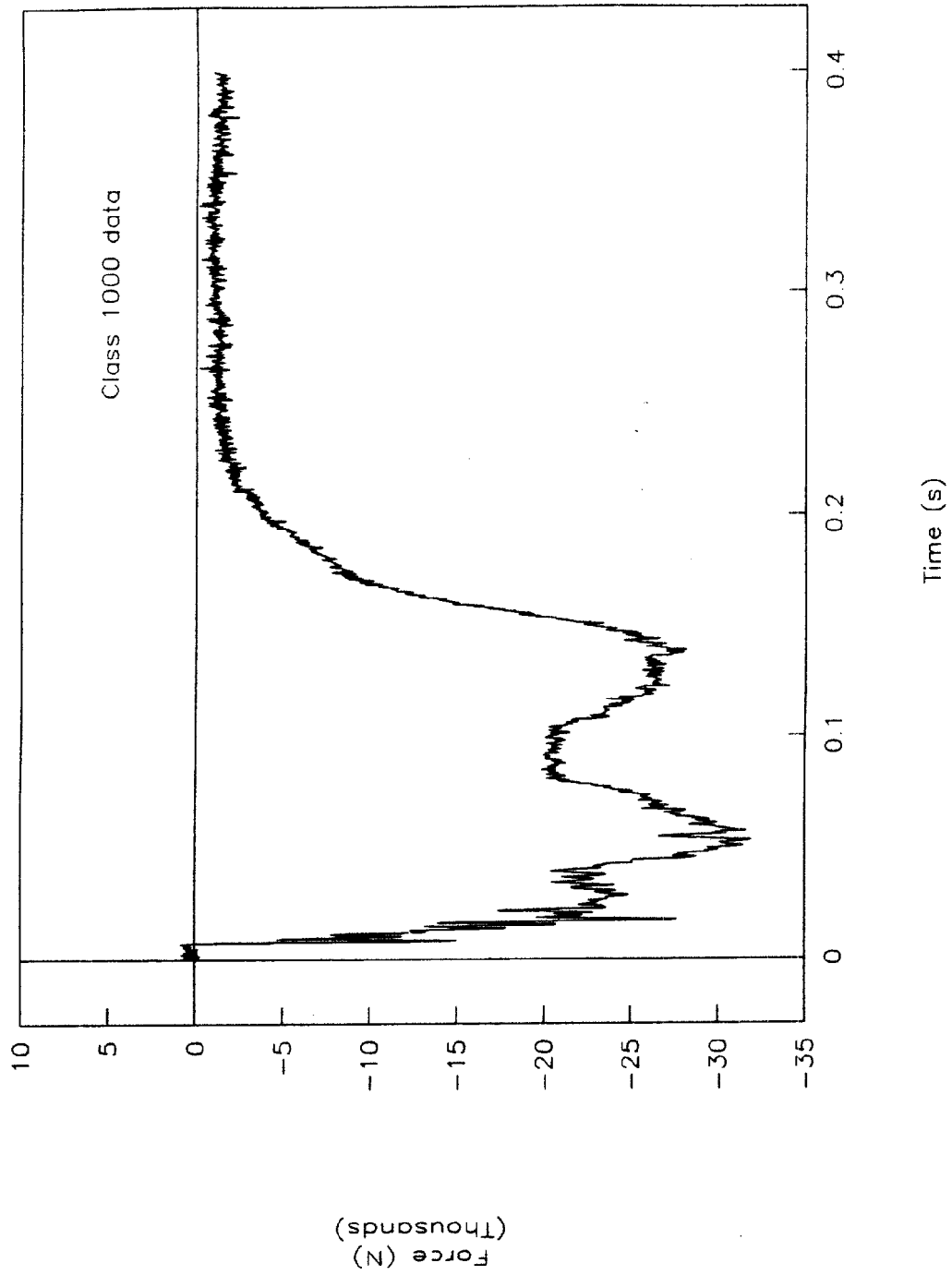


Figure 40. Rigid pole, force vs. time, bottom face upper load cell, test 97S003.

Test No. 97S003

Lower-middle face lower load cell

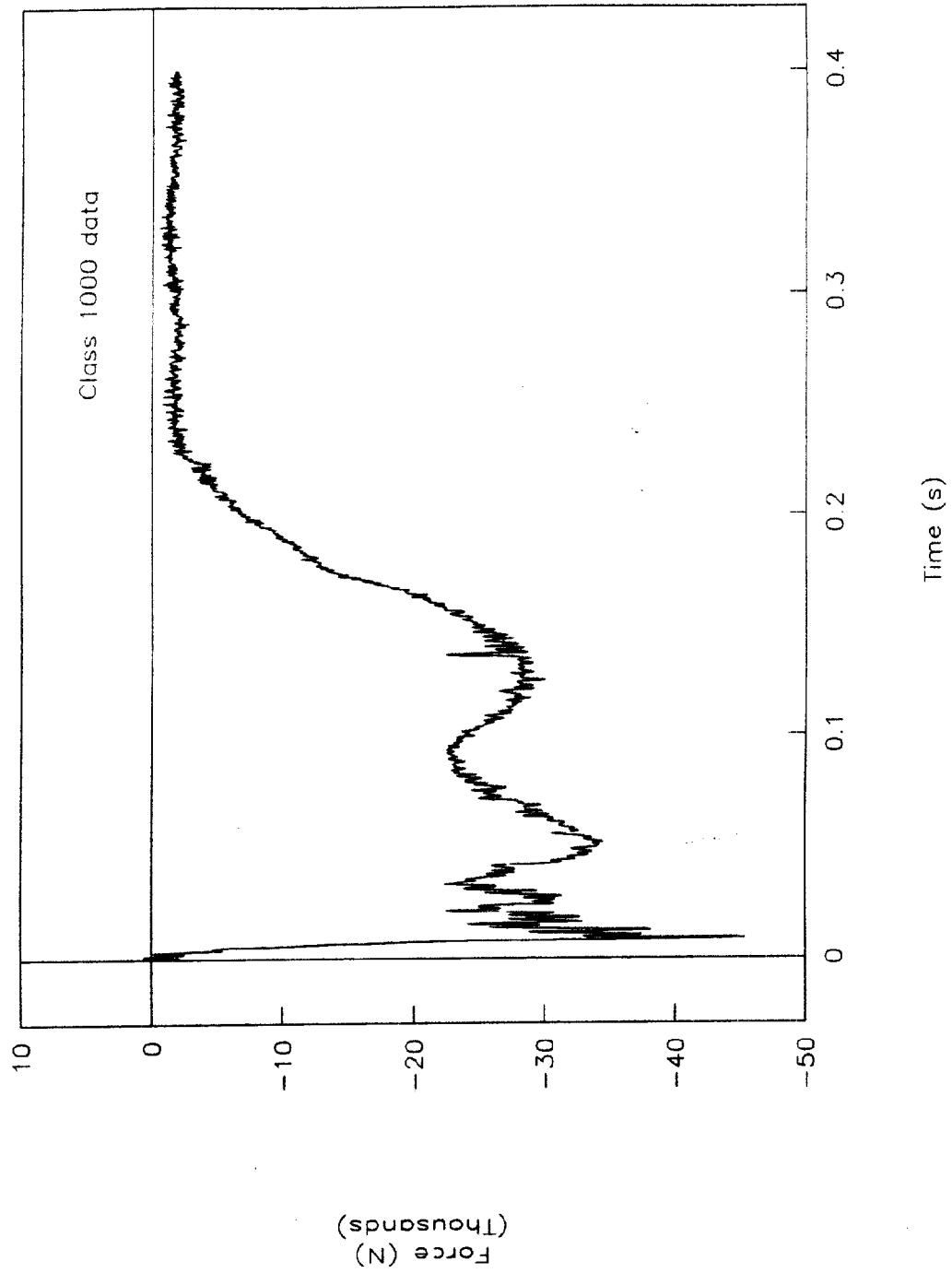


Figure 41. Rigid pole, force vs. time, lower-middle face lower load cell, test 97S003.

Test No. 97S003

Lower-middle face upper load cell

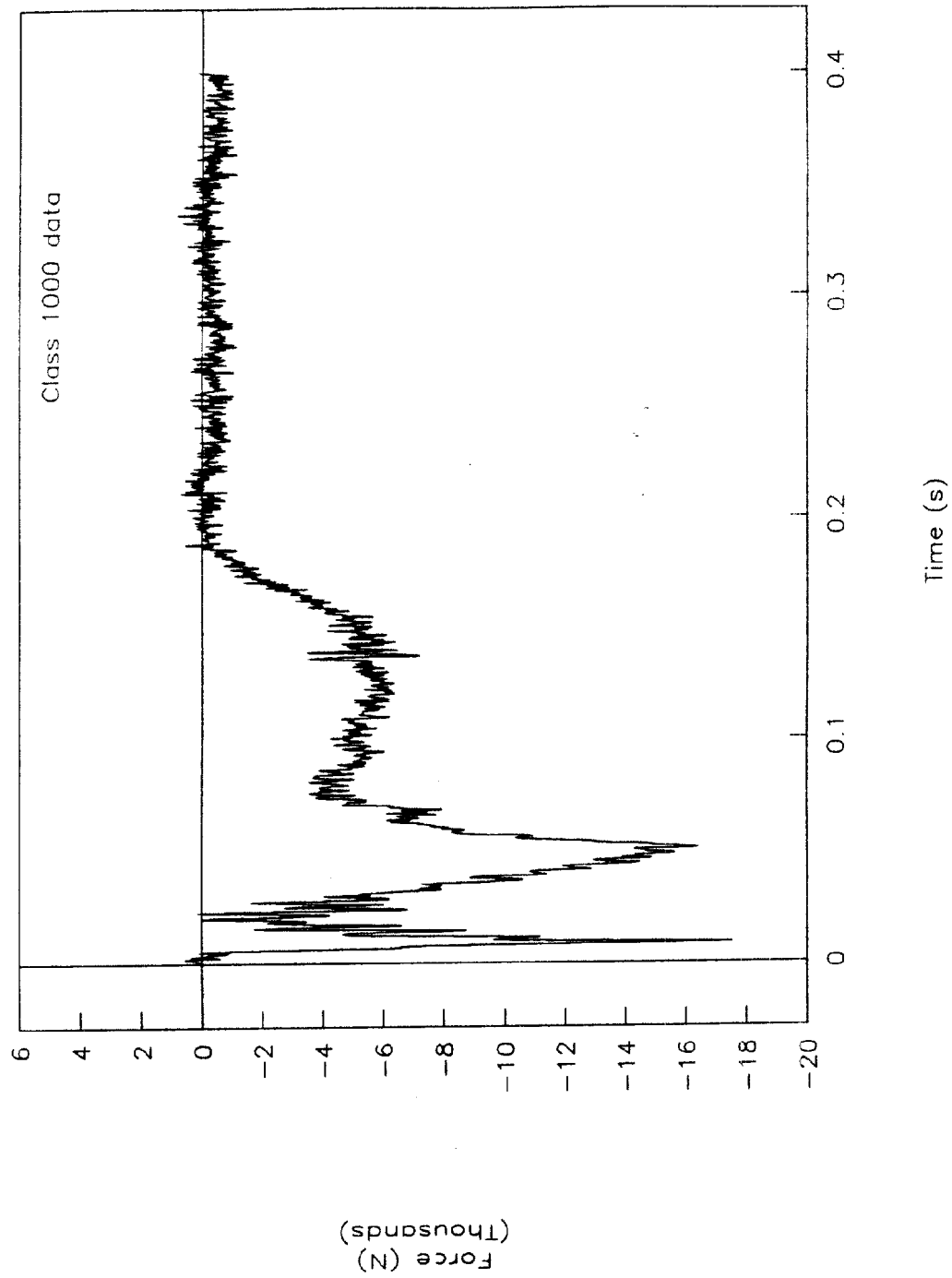


Figure 42. Rigid pole, force vs. time, lower-middle face upper load cell, test 97S003.

Test No. 97S003

Upper-middle face lower load cell

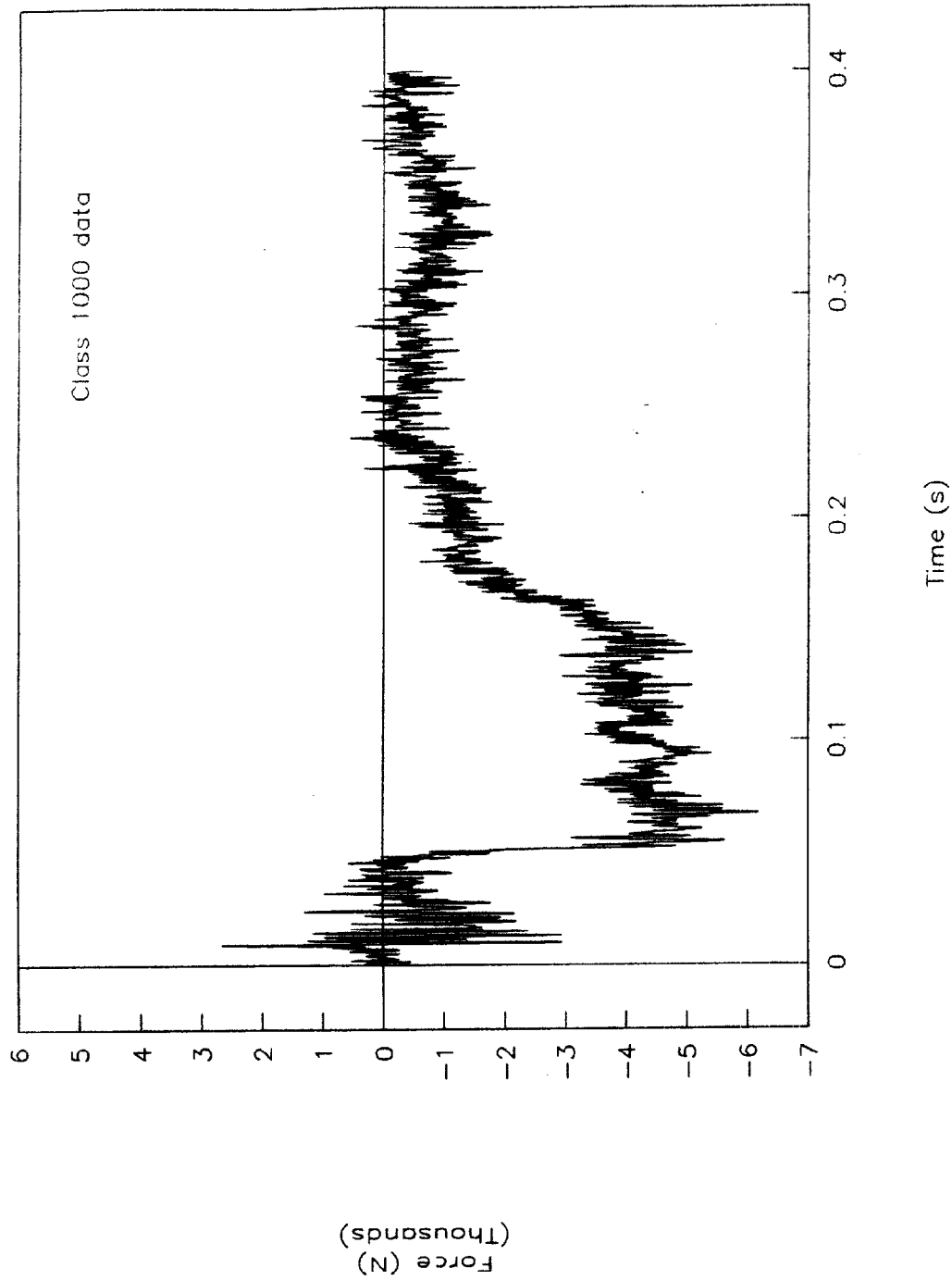


Figure 43. Rigid pole, force vs. time, upper-middle face lower load cell, test 97S003.

Test No. 97S003

Upper-middle face upper load cell

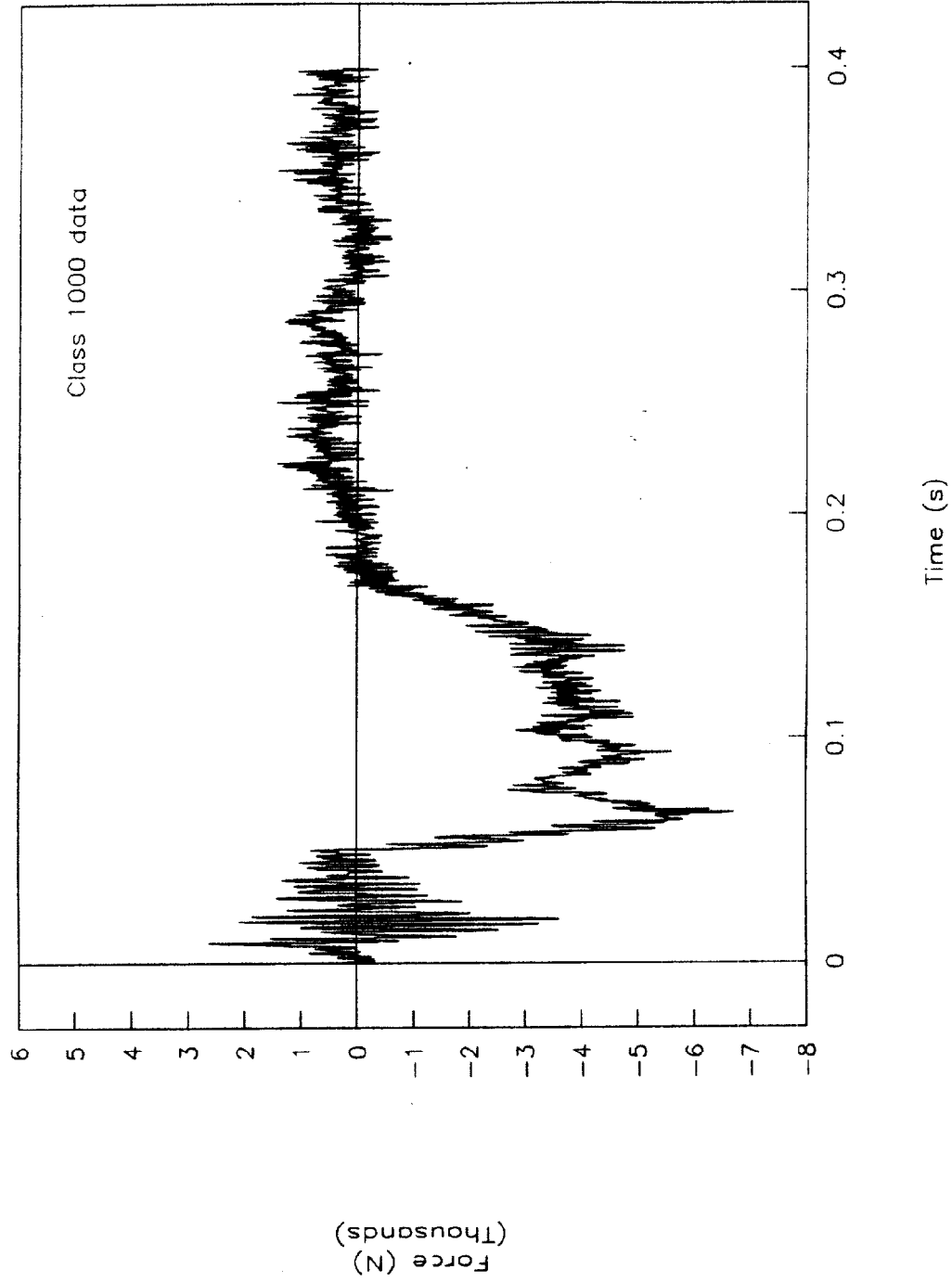


Figure 44. Rigid pole, force vs. time, upper-middle face upper load cell, test 97S003.

Test No. 97S003

Upper face lower load cell

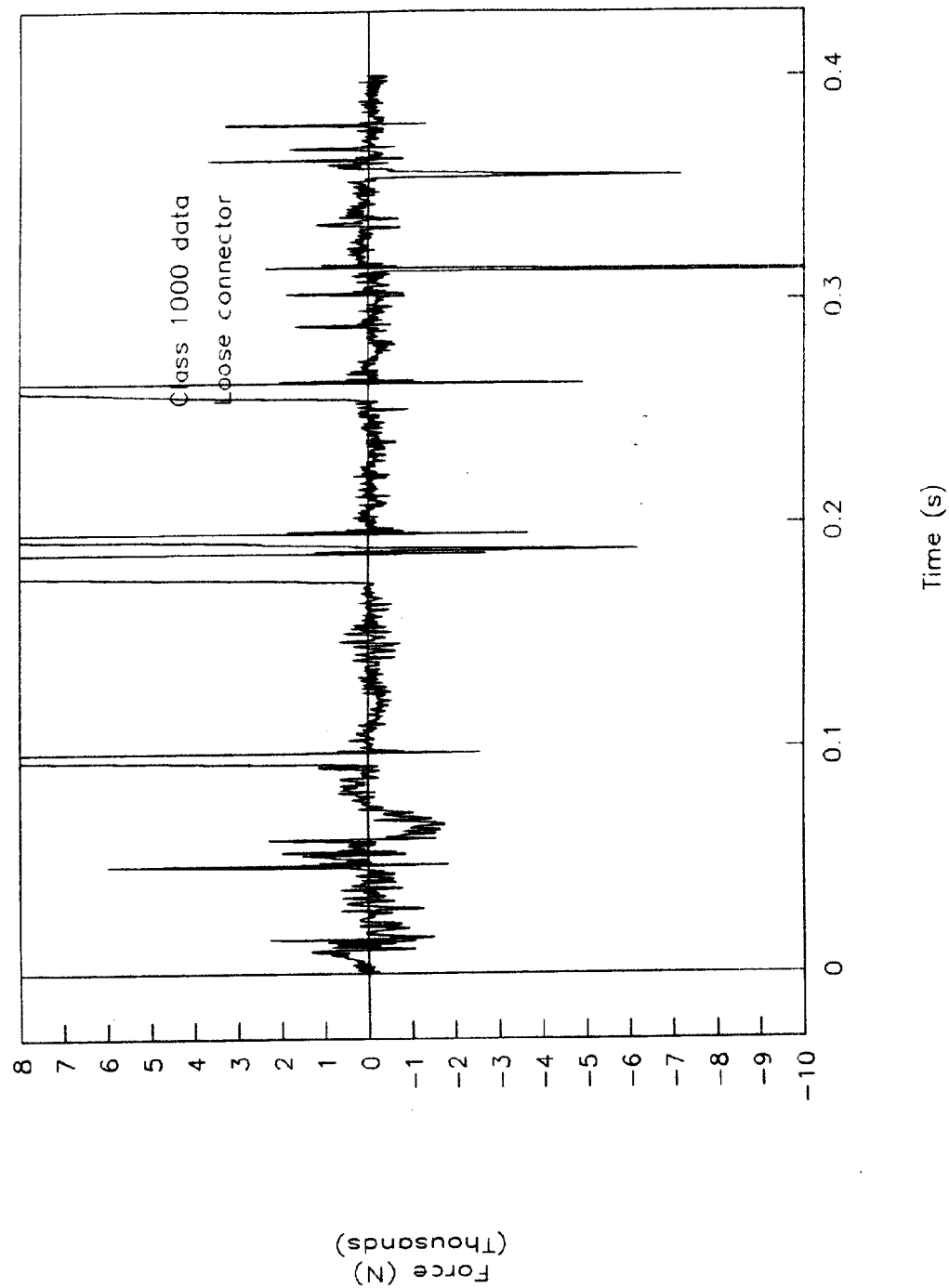


Figure 45. Rigid pole, force vs. time, upper face lower load cell, test 97S003.

Test No. 97S003

Upper face upper load cell

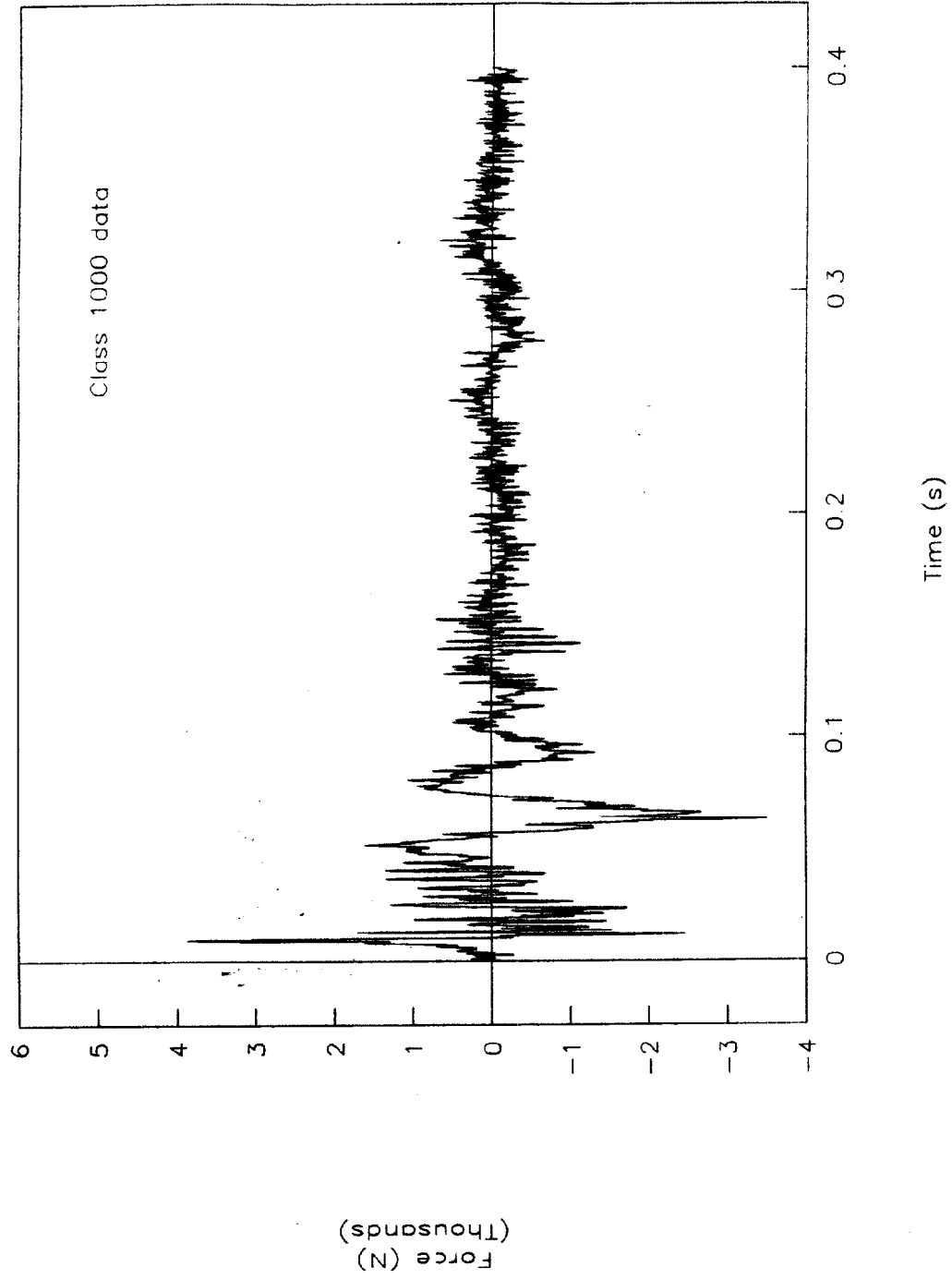


Figure 46. Rigid pole, force vs. time, upper face upper load cell, test 97S003.

REFERENCES

Number

- (1) NHTSA. *Laboratory Test Procedure for Federal Motor Vehicle Safety Standard 201*, National Highway Traffic Safety Administration, Washington, DC, April 1997.
- (2) NHTSA. *Laboratory Test Procedure for Federal Motor Vehicle Safety Standard 214*, National Highway Traffic Safety Administration, Washington, DC, May 1992.

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- (1) NHTSA. *Laboratory Test Procedure for Federal Motor Vehicle Safety Standard 201*, National Highway Traffic Safety Administration, Washington, DC, April 1997.
- (2) NHTSA. *Laboratory Test Procedure for Federal Motor Vehicle Safety Standard 214*, National Highway Traffic Safety Administration, Washington, DC, May 1992.
- (3) Christopher M. Brown, *Honda Accord LX Broadside Collision with a Narrow Fixed-Object: FOIL Test Number 97S003*, Report Number FHWA-RD-98-008, Federal Highway Administration, Washington, DC, January 1998.
- (4) Christopher M. Brown, *Honda Accord LX Broadside Collision with a Narrow Fixed-Object: FOIL Test Number 97S004*, Report Number FHWA-RD-98-009, Federal Highway Administration, Washington, DC, January 1998.
- (5) Christopher M. Brown, *Honda Accord LX Broadside Collision with a Narrow Fixed-Object: FOIL Test Number 97S005*, Report Number FHWA-RD-98-010, Federal Highway Administration, Washington, DC, January 1998.